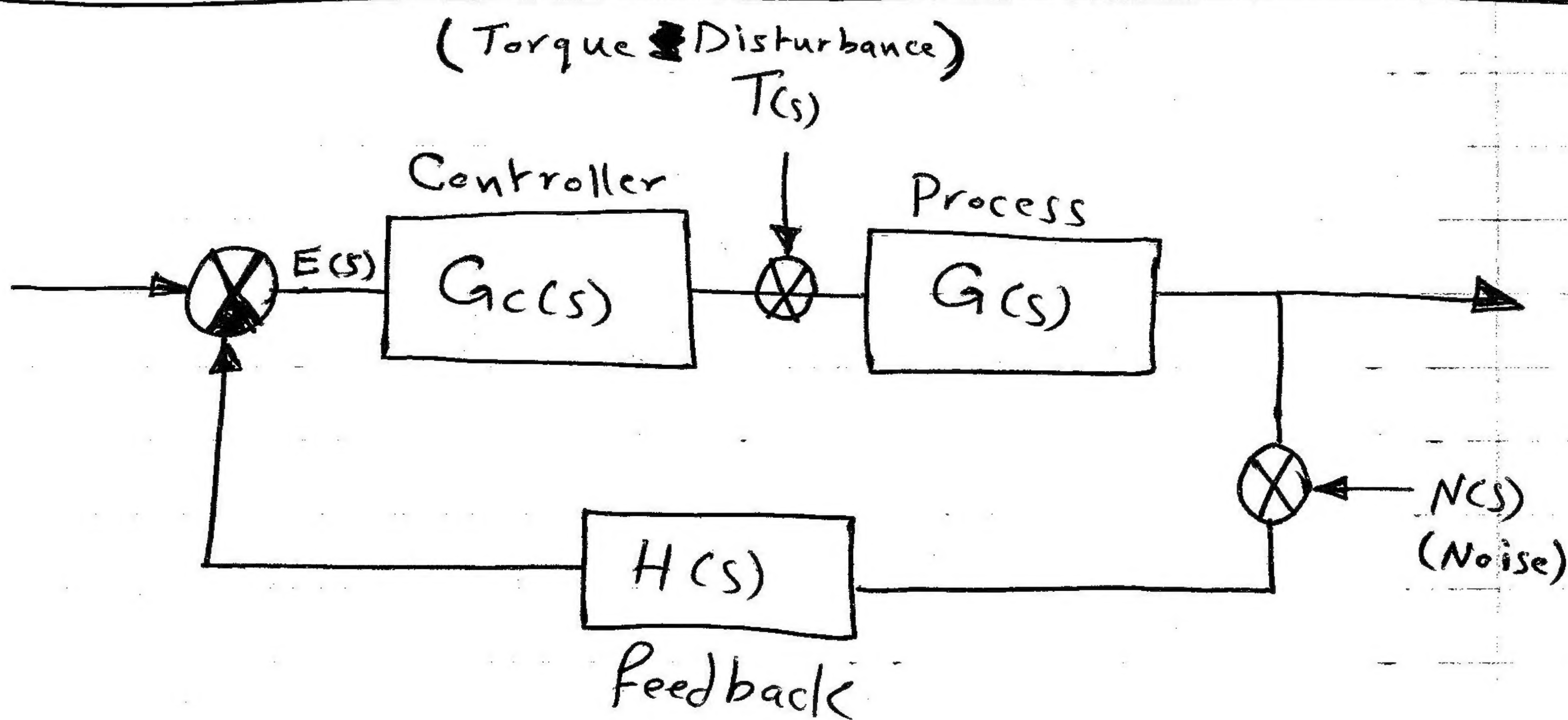


The Steady State Error of a feedback Control System



$$E(s) = R(s) - C(s) H(s) \implies H(s) = 1$$

$$\therefore E(s) = R(s) - C(s)$$

$$\otimes E(s) = R(s) - C(s)$$

$$H(s) = 1$$

$$= R(s) \left[1 - \frac{C(s) H(s)}{R(s)} \right]$$

$$= R(s) \left[1 - \frac{G_c(s) G(s) H(s)}{1 + G_c(s) G(s) H(s)} \right]$$

$$= R(s) \left[\frac{1 + G_c(s) G(s) H(s) - G_c(s) G(s) H(s)}{1 + G_c(s) G(s) H(s)} \right]$$

$$= \frac{1}{1 + G_c(s) G(s) H(s)} * R(s)$$

1

⊛ If $R(s) = \frac{A}{s}$ (Step Input).

$$E(s) = \frac{A/s}{1 + G(s)G(s)H(s)}$$

$$e_{ss} = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} s E(s)$$

$$= \lim_{s \rightarrow 0} s * \frac{A/s}{1 + G(s)G(s)H(s)}$$

$$= \frac{A}{1 + G(s)G(s)H(s)}$$

⊛ The Loop transfer function is given by :-

$$G(s)G(s)H(s) = \frac{k \prod_{i=1}^M (s - z_i)}{s^N \prod_{k=1}^Q (s - p_k)}$$

~~z_i : أصف - قطب~~ z_i : أصف - قطب p_k : أصف - مقام

Ex

$$\frac{2}{3s^2} \times \frac{3(s+1)}{s^2+1} \times \frac{(s-2)}{s^3+s+1} = \frac{6(s+1)(s-2)}{3s^2(s^2+1)(s^3+s+1)}$$

⊛ k : حاصل قسمة ثابت الذي في البسط على ثابت الذي في المقام

$$\text{total Gain} \leftarrow \textcircled{2} = \frac{6}{3} = k \text{ في المثال السابق}$$

⊕ The No of integration is often indicated by Labeling a system with a type Number that is equal to N .

⊕ The steady State tracking error for a step input of magnitude "A" is given by :-

$$e_{ss} = \frac{A}{1+K_p} \quad \text{for type Zero.}$$

⊕ K_p : Positioning Constant

⊕ If the system has more than one integration, then

$$e_{ss} = \text{Zero}$$

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$$E(s) = \frac{R(s)}{1+G_c(s)G(s)H(s)}$$

2

⊕ If $R(s) = \text{Ramp input} = \frac{A}{s^2}$

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s^2}{1+G_c(s)G(s)H(s)} = \lim_{s \rightarrow 0} \frac{A}{sG_c(s)G(s)H(s)}$$

⊗ If the system is type Zero $\Rightarrow N=0$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s \times k} = \frac{A}{0} = \infty$$

⊛ If the system is type 1 $\Rightarrow N=1$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s * \frac{K_v}{s}} = \boxed{A/K_v}$$

K_v : Velocity Constant

$$G_c(s) G(s) H(s) = \frac{K \prod_{i=1}^M (s - z_i)}{s^N \prod_{k=1}^Q (s - p_k)}$$

⊛ If the system is type 2 $\Rightarrow N=2$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s * \frac{k}{s^2}} = \frac{A}{\frac{k}{s}} = \frac{A}{\infty} = \boxed{\text{Zero}}$$

In the case of Ramp Input, we need two

Integrators to eliminate the error.

⊛ [3] If $R(t) = \frac{At^2}{2} \Rightarrow R(s) = \frac{A}{s^3}$

“Acceleration Input”

$$E(s) = \frac{R(s)}{1 + G_c(s) G(s) H(s)} = \frac{A/s^3}{1 + G_c(s) G(s) H(s)}$$

$$e_{ss} = \lim_{s \rightarrow 0} s^1 \frac{A/s^3}{1 + G_c(s) G(s) H(s)} = \lim_{s \rightarrow 0} \frac{A}{s^2 G_c(s) G(s) H(s)}$$

□ $N=0 \Rightarrow e_{ss} = \infty$

$N=1 \Rightarrow e_{ss} = \infty$

$N=2 \Rightarrow e_{ss} = \frac{A}{K_a}$

$N=0 \Rightarrow G_c G H(s) = K_1$

$N=1 \Rightarrow G_c G H(s) = \frac{K_2}{s}$

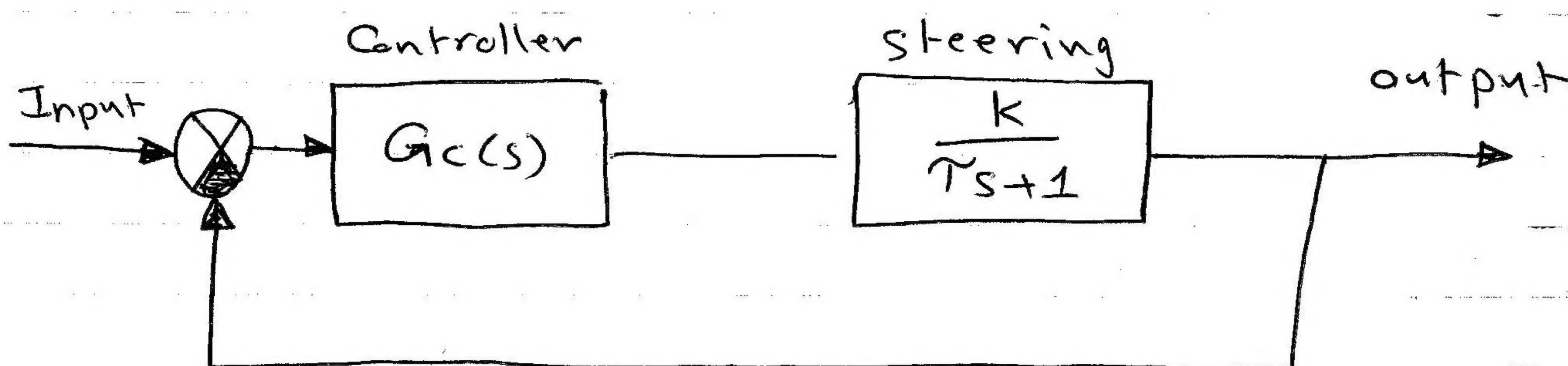
$N=2 \Rightarrow G_c G H(s) = \frac{K_3}{s^2}$

K_a = Acceleration Constant

Type \ Input	Unit step $r(t) = A$ $R(s) = A/s$	Ramp Input $r(t) = At$ $R(s) = A/s^2$	Acceleration Input $r(t) = At^2/2$ $R(s) = A/s^3$
$N=0$	$\frac{A}{1+K_p}$	∞	∞
$N=1$	Zero	$\frac{A}{K_v}$	∞
$N=2$	Zero	Zero	$\frac{A}{K_a}$

Ex: Mobile Robot may be designed as an assisting device or servant for disabled person.

- The steering Control system for a such robot can be represented by



here we used PI- Controller
"given in the question"

Case 1 : If $R(s) = \text{Unit Step Input} = \frac{A}{s}$

$$\text{If } G_c(s) = \frac{k_1 s + k_2}{s} = \boxed{\frac{k_1 + \frac{k_2}{s}}{s}}$$

↑ ↑
P I Controller

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s}{1 + G_c G H(s)} = \frac{A}{1 + G_c G H(s)}$$

$$G_c G H(s) = \frac{k_1 s + k_2}{s} * \frac{k}{\tau s + 1} = \frac{k_2 * k}{s}$$

$$\therefore e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s}{1 + G_c G H(s)} = \frac{A}{1 + G_c G H(s)} = \frac{A}{1 + \frac{k_2 k}{s}} = \boxed{\text{Zero}}$$

Case 2 : If $R(s) = \text{Ramp Input} = \frac{A}{s^2}$

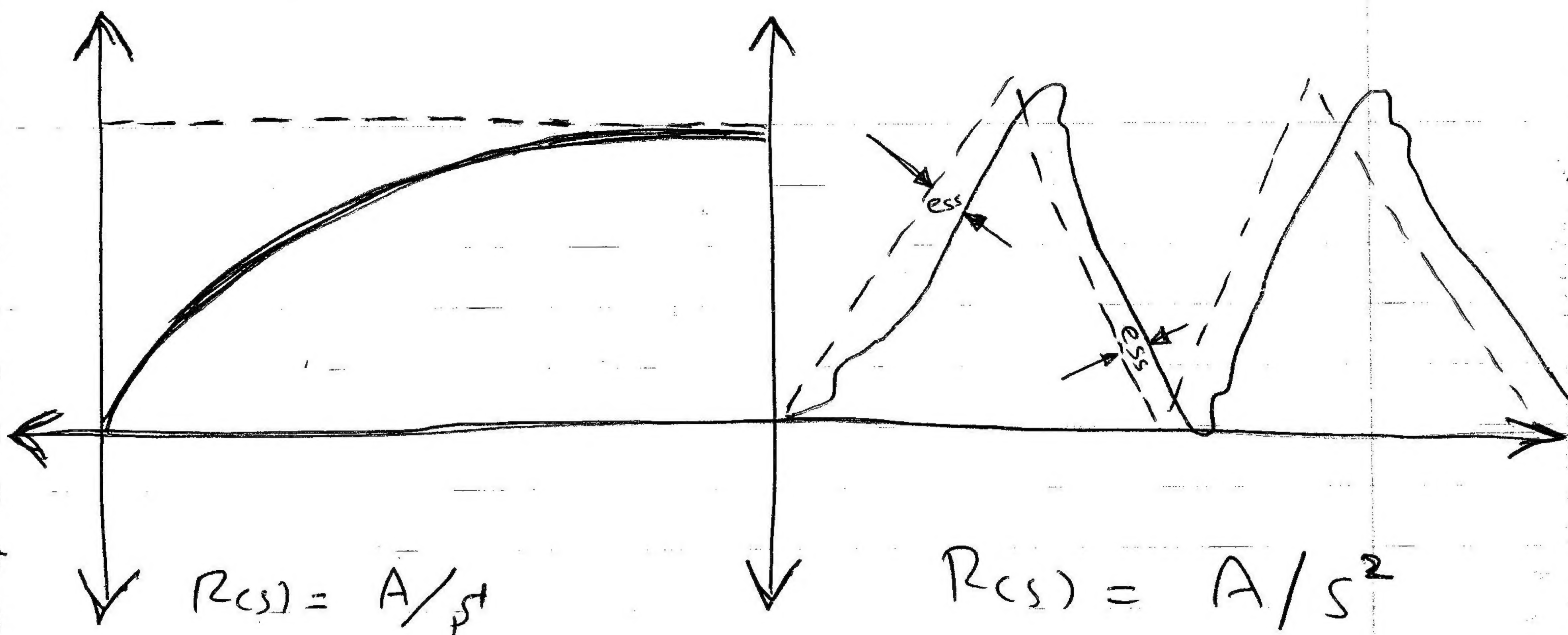
With PI Controller

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s^2}{1 + G_c G H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{A}{s G_c G H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{A}{s * \frac{k_2 k}{s}} = \boxed{\frac{A}{k_2 k}}$$

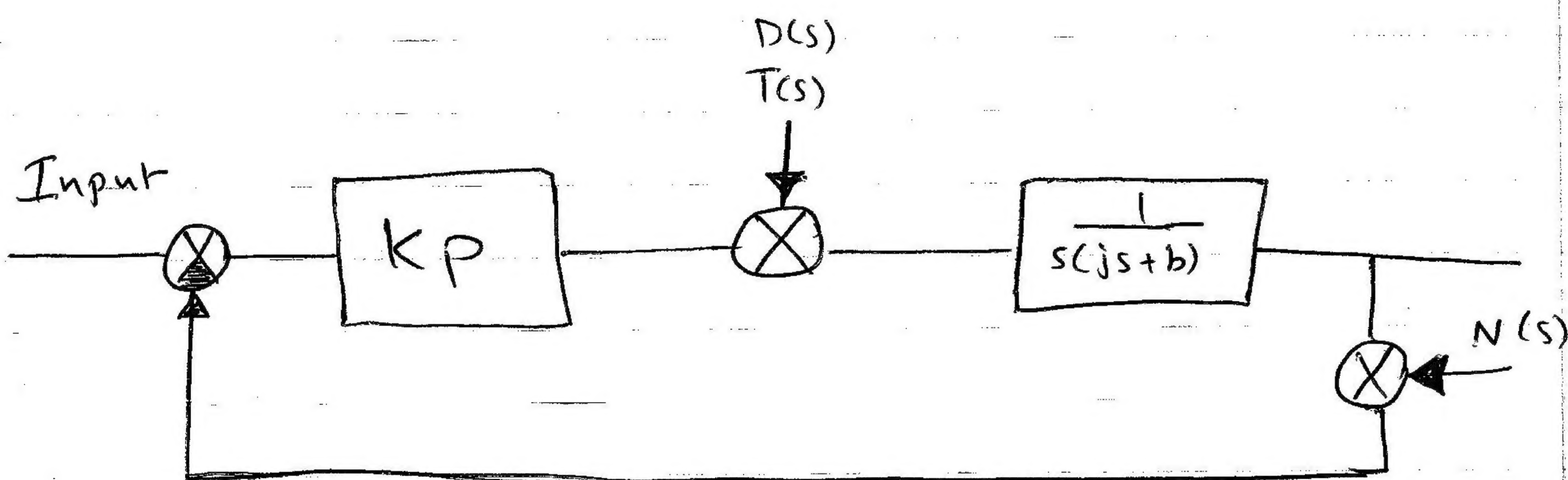
$k_2 k$: Velocity Constant



In the case of Ramp Input, we need two Integrators to Eliminate the error.

11/26 SCW

① Response to torque (Proportional Controller)

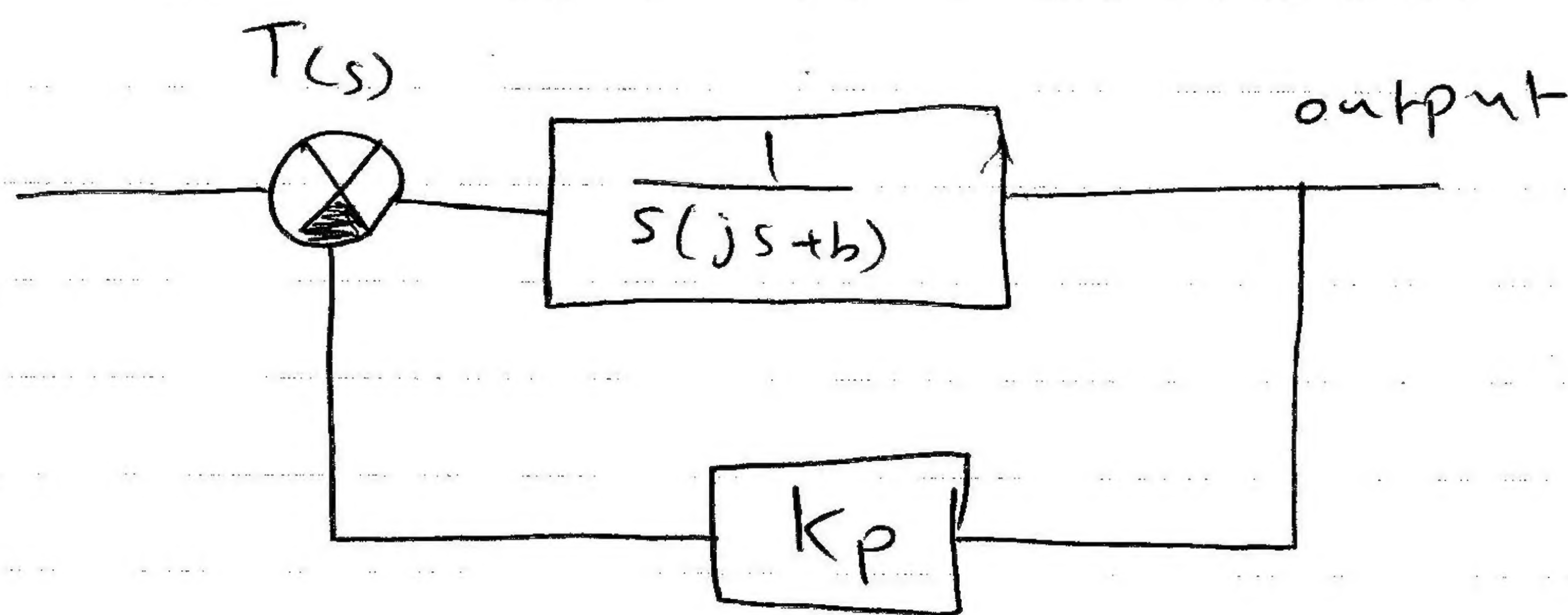


- ① Set Input to Zero
- ② Set $N(s) = \text{Zero}$
- ③ Rearrange the control diagram

Input = 0

$$N(s) = 0$$

⇒ Now Rearrange the control diagram as follows:-



$$\otimes E(s) = \text{Input} - \text{Output}$$

$$= \text{Zero} - \text{Output}$$

$$= \text{Zero} - C(s) = \boxed{-C(s)}$$

$$\otimes \frac{C(s)}{D(s)} = \frac{\frac{1}{s(js+b)}}{\frac{1}{s(js+b)} * k_p + 1} = \frac{1}{s(js+b) + k_p}$$
$$= \boxed{\frac{1}{js^2 + bs + kp}}$$

$$\otimes \therefore \frac{E(s)}{D(s)} = \frac{-C(s)}{D(s)} = \boxed{\frac{-1}{js^2 + bs + kp}}$$

$$\therefore E(s) = \boxed{\frac{-Ds}{js^2 + bs + kp}}$$

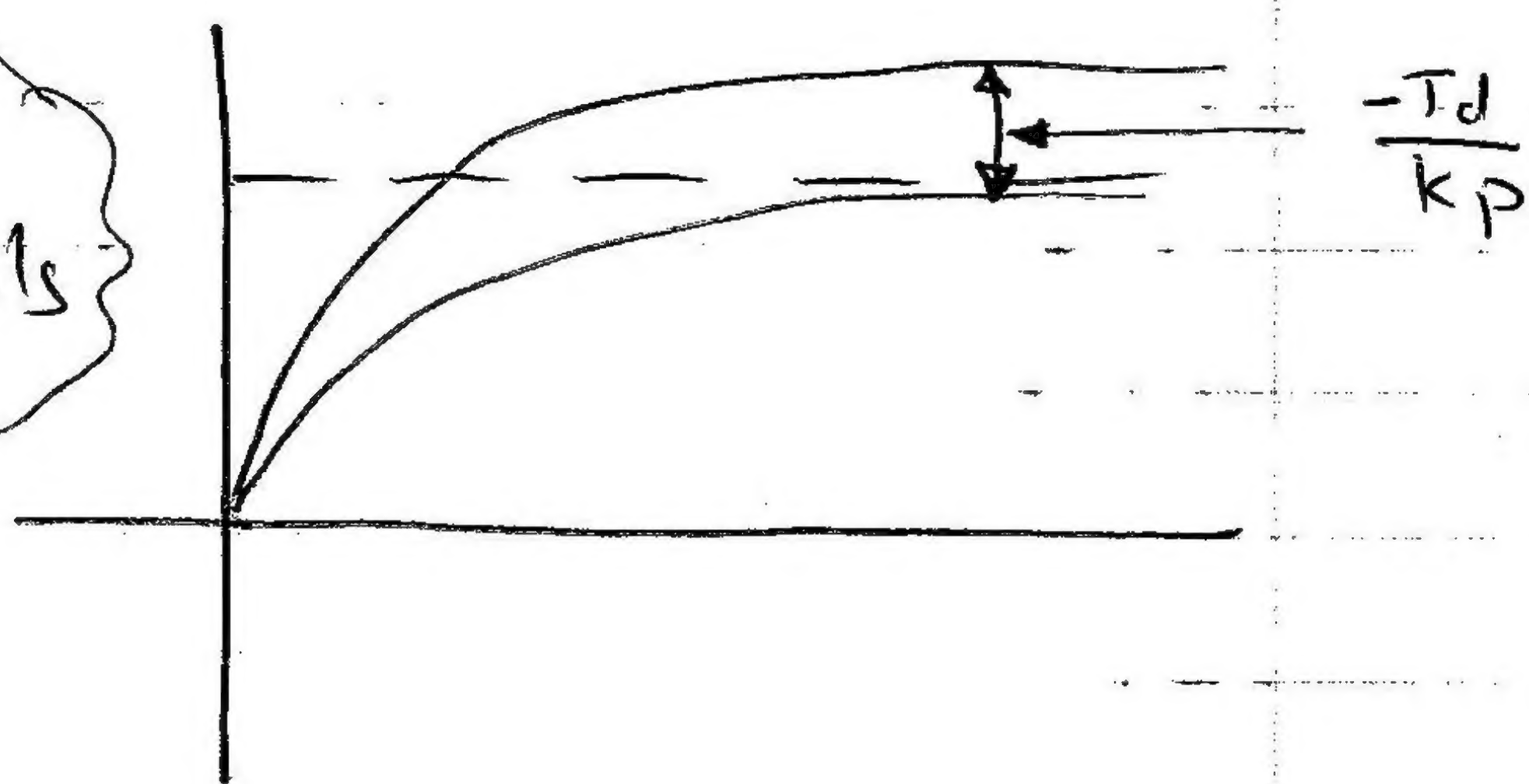
$D(s)$ is a unit Step disturbance $\Rightarrow D(s) = \frac{T_d}{s}$

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{-\frac{T_d}{s}}{js^2 + bs + kp}$$

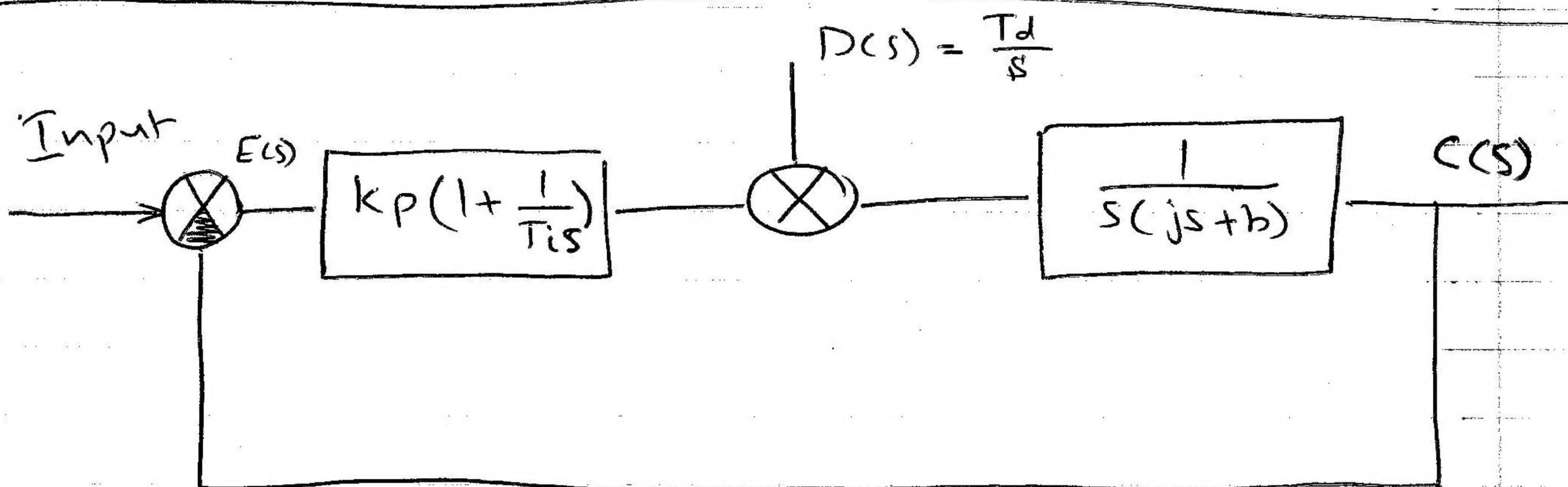
$$= \lim_{s \rightarrow 0} \frac{-T_d}{js^2 + bs + kp} = \frac{-T_d}{j(0)^2 + b(0) + kp}$$

$$= \boxed{\frac{-T_d}{kp}}$$

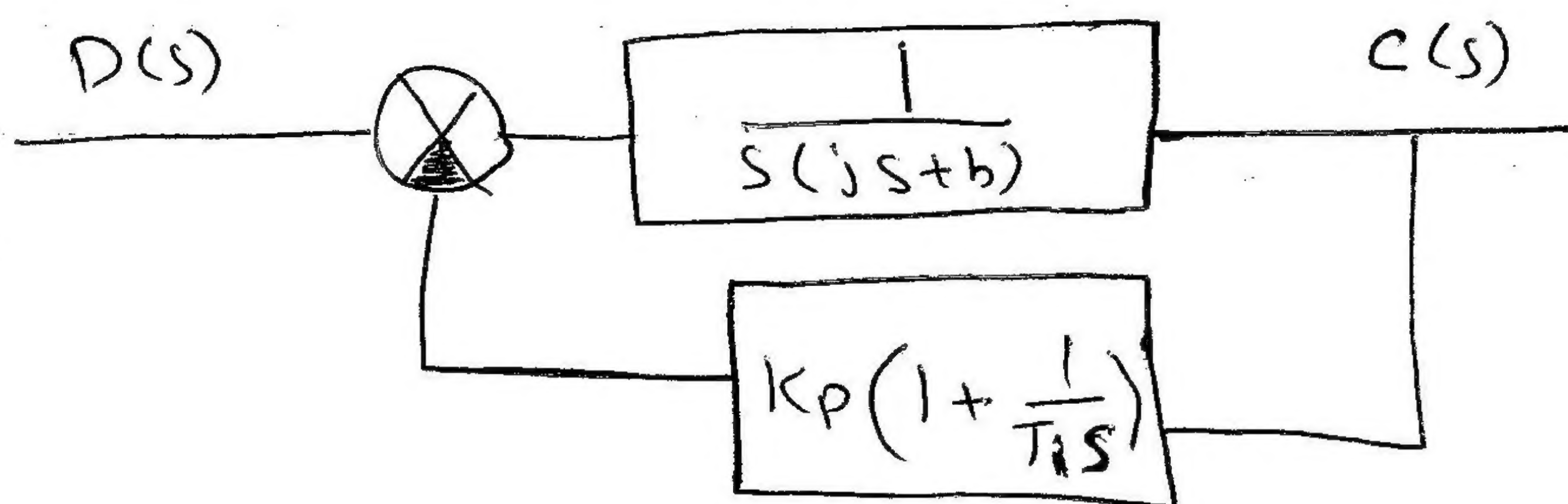
∴ The P-controller Cannot eliminate the error and equals it to zero, but it can decrease the error.



② Response to torque (PI-Controller)



\Rightarrow Rearrange the Control diagram \circ (input = zero)



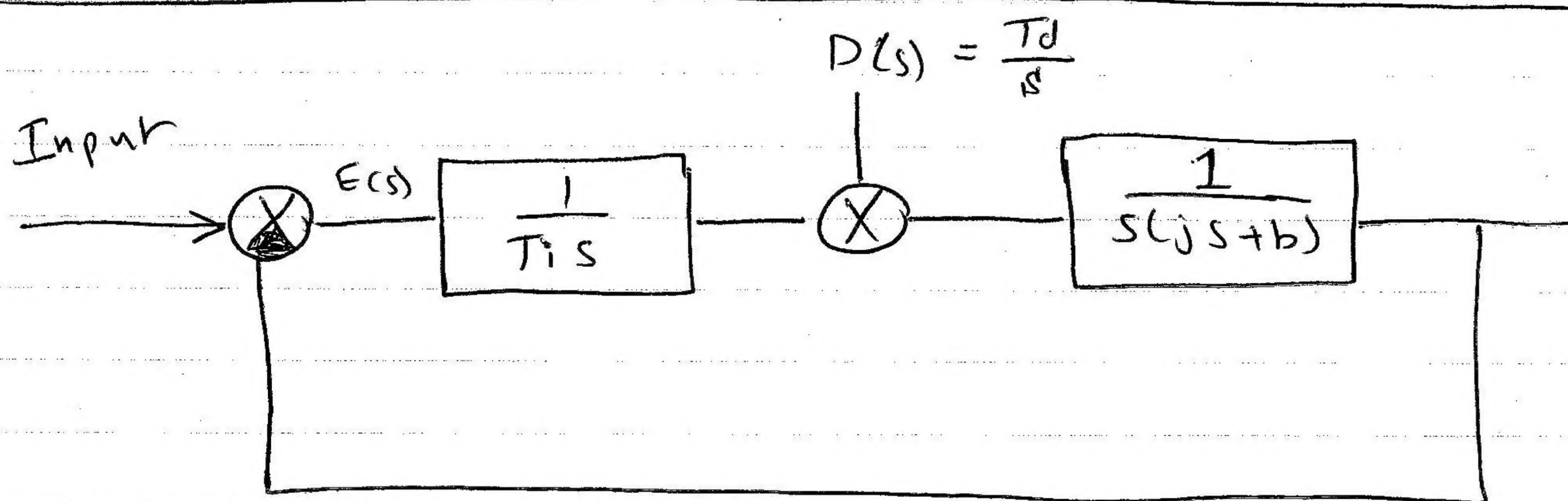
$$\lim_{s \rightarrow 0} \frac{E(s)}{D(s)} = \frac{-s}{Js^3 + bs^2 + kps + \frac{kp}{Ti}}$$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} s \frac{-s \frac{T_d}{s}}{Js^3 + bs^2 + kps + \frac{kp}{Ti}}$$

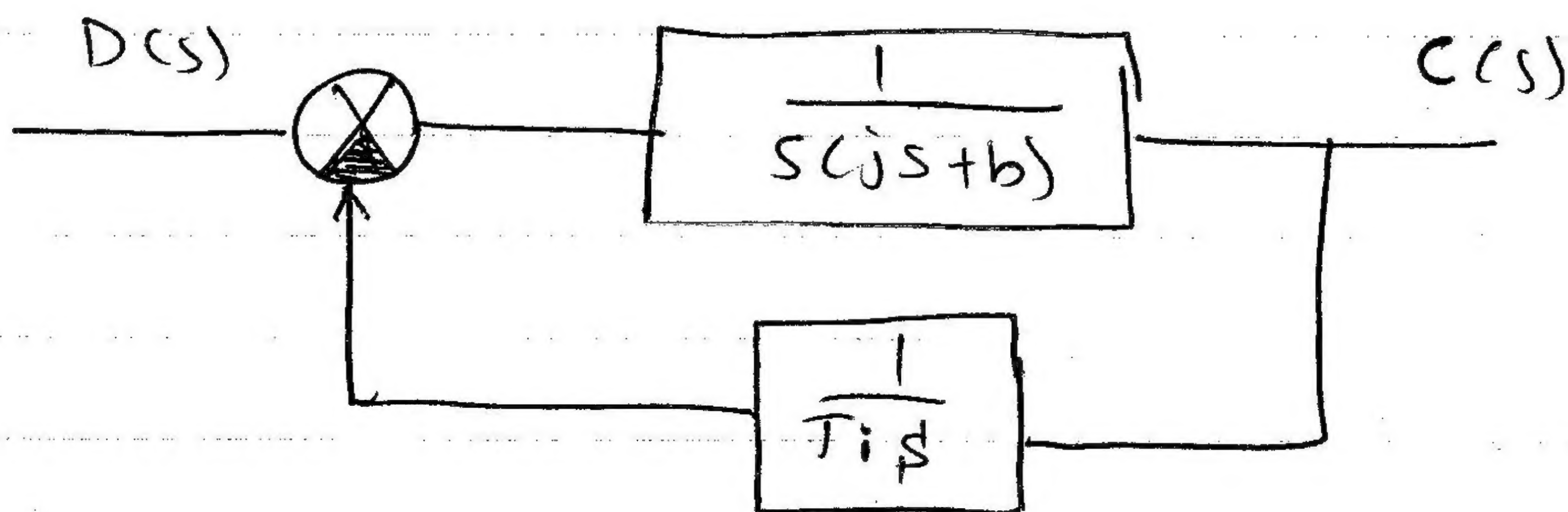
$$= \boxed{\text{Zero}}$$

∴ Using the PI-Controller eliminate the error

③ Response to torque (I-Controller only)



⇒ Rearrange the control diagram (Input = 0)



$$\begin{aligned}
 \frac{C(s)}{D(s)} &= \frac{1}{s(j s + b)} = \frac{1}{\frac{1}{s(j s + b)} * \frac{1}{T_i s} + 1} = \frac{1}{\frac{1}{T_i s} + s(j s + b)} \\
 &= \frac{T_i s}{1 + T_i s^2(j s + b)} \\
 &= \frac{T_i s}{1 + T_i j s^3 + T_i b s^2} = \frac{C(s)}{D(s)}
 \end{aligned}$$

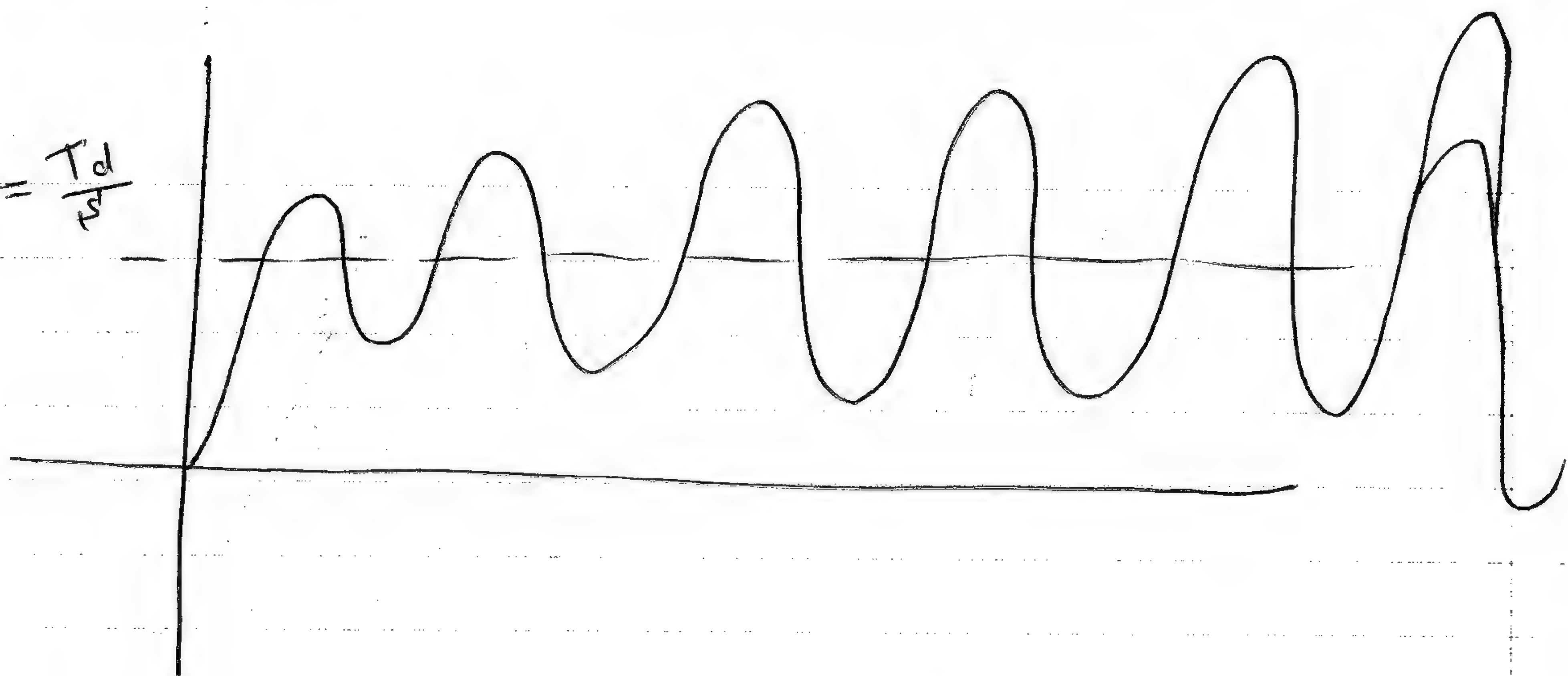
$$\begin{aligned}
 \infty e_{ss} &= \lim_{s \rightarrow 0} s \frac{T_i s * \frac{T_d}{s}}{1 + T_i j s^3 + T_i b s^2} \\
 &= \boxed{\text{Zero}}
 \end{aligned}$$

$$\frac{C(s)}{D(s)} = \frac{T_i s}{T_i j s^3 + T_i b s^2 + 1}$$

s^3	$T_i j$	0
s^2	$T_i b$	1
s	$\left(\frac{-j}{b}\right)$	0
1	1	

The system is unstable !!

$$D(s) = \frac{T_d}{s}$$



⊛ :- We must Use PI-Controller to eliminate the error and to maintain the stability of the system.

⊛ Using I-Controller only eliminate the errors but the system is "Unstable".

Performance Indices

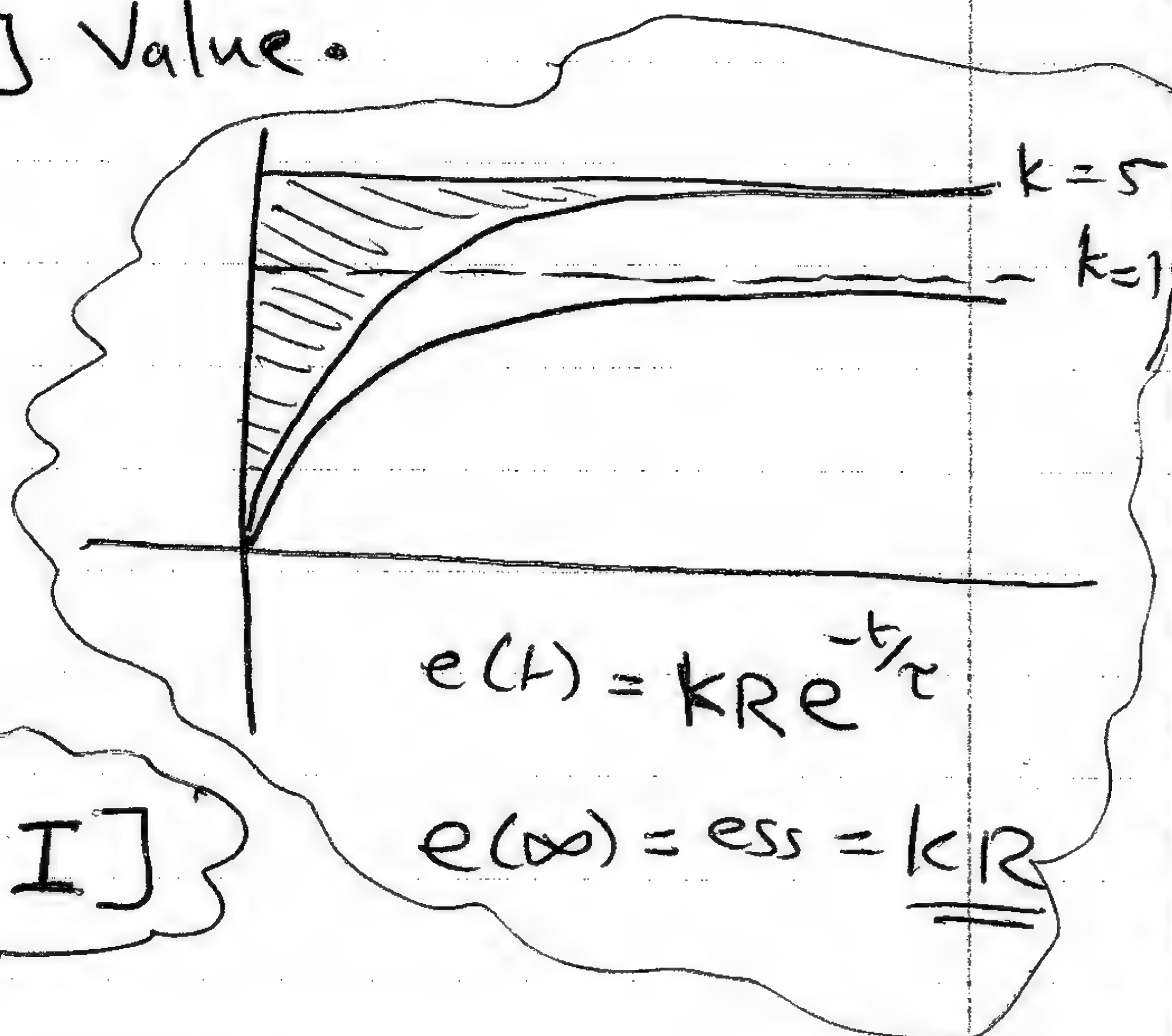
[Dorf 5.7]

⊗ A performance index J is a quantitative measure of the performance of a system, and is chosen so that emphasis is given to the important system specifications

⊗ a system is ~~is~~ considered an Optimum Control System when the system parameters are adjusted so that the index reaches its extremum [minimum] value.

⊗ a performance Index must be a number that is always Positive

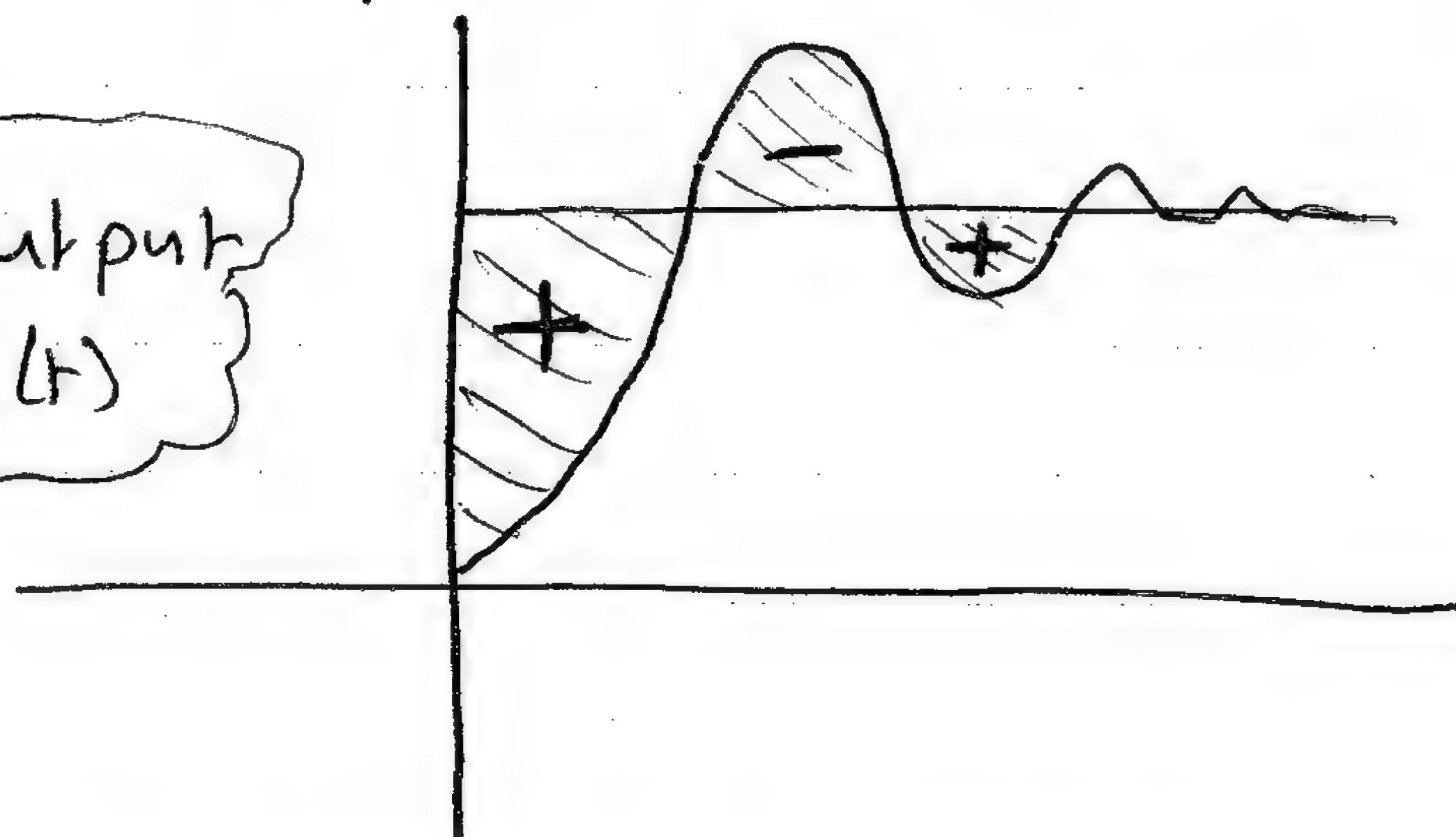
Performance Index Symbol : $[I]$



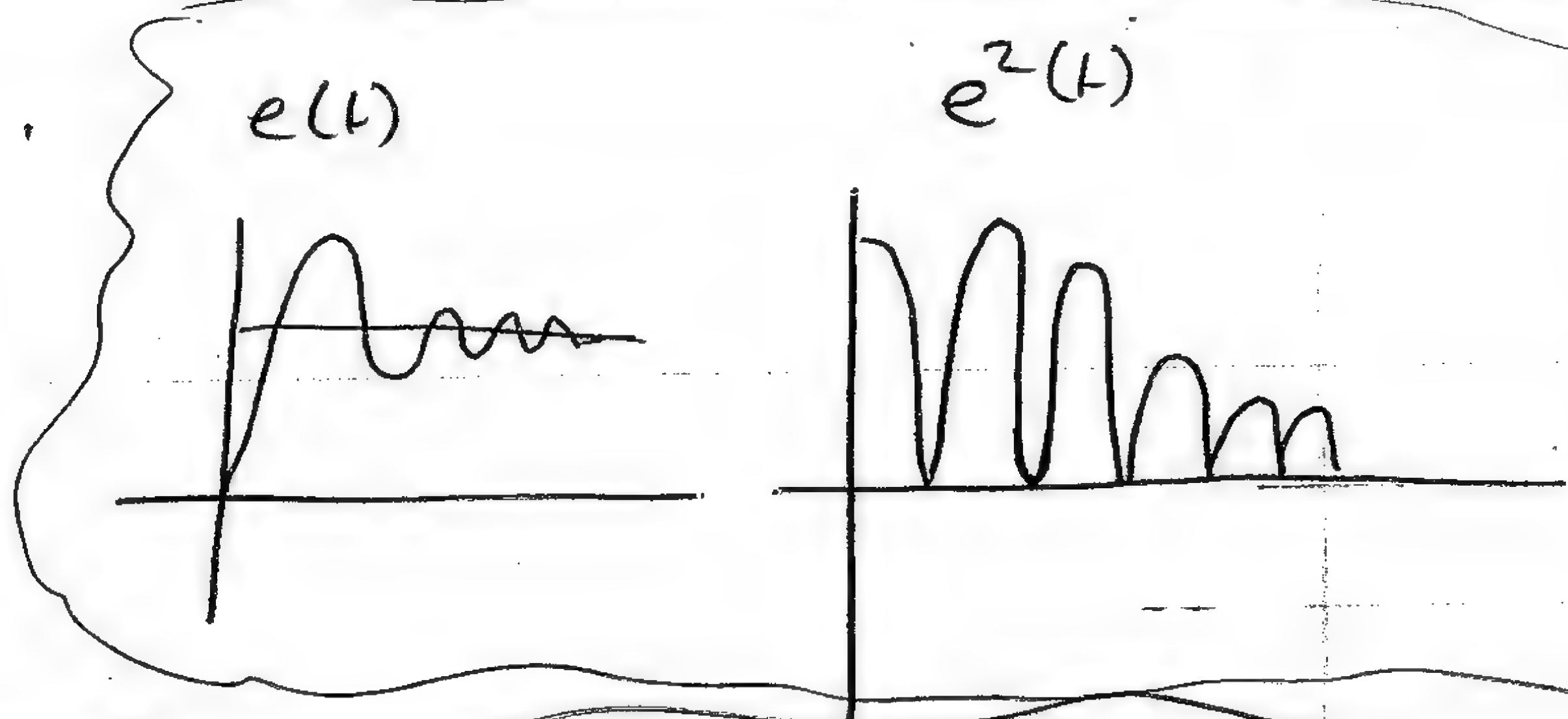
Error Criterion J -

1. Integral of the Square of the error (ISE)

error = Input - output
 $= R(t) - C(t)$

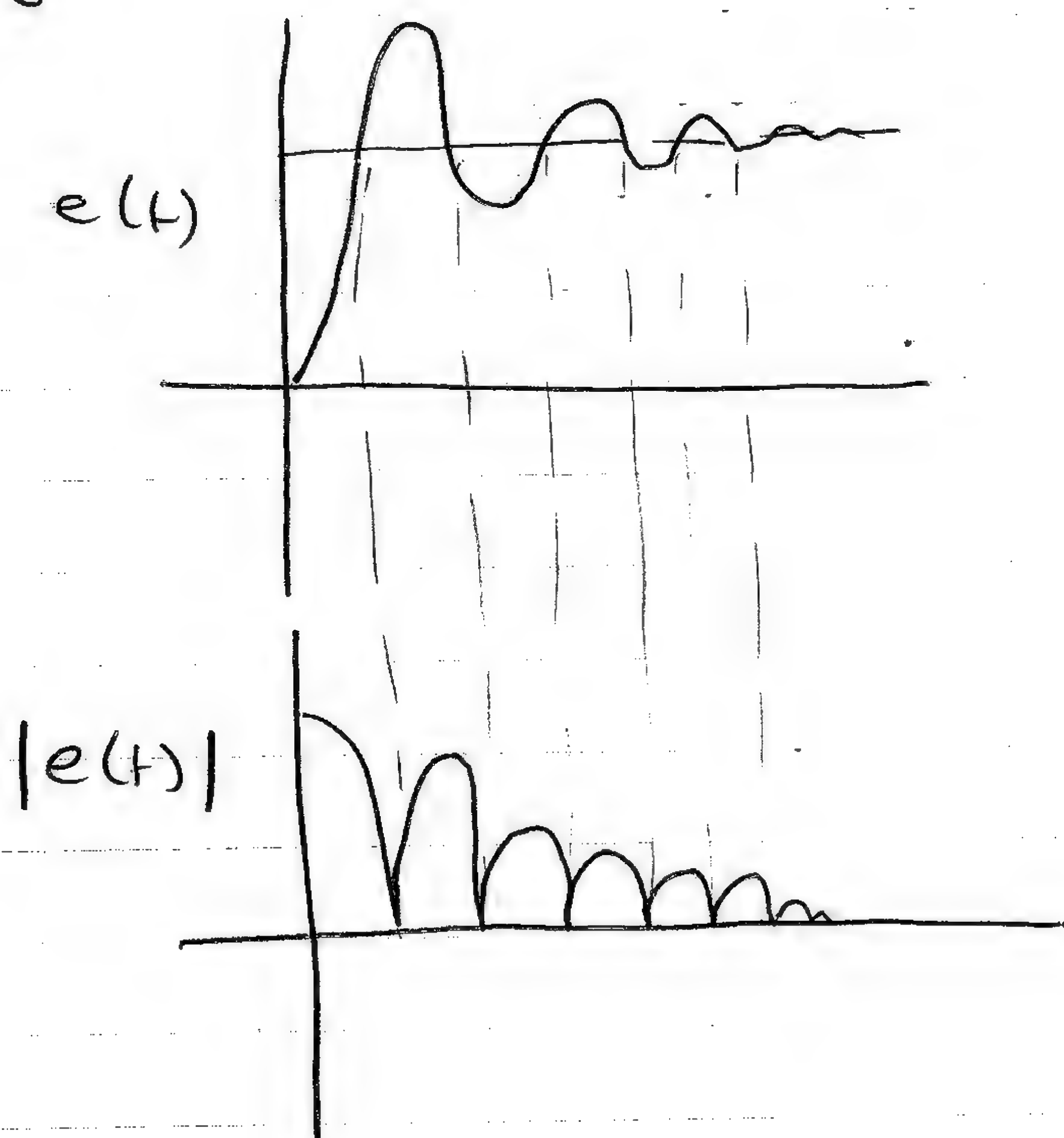


$$I = \int_0^{T_s (T_s \text{ or } \infty)} e^2(t) \cdot dt$$



2. Integral of the absolute value of the error (IAE)

$$I = \int_0^{T_s (T_s \text{ or } \infty)} |e(t)| dt$$



3. Integral of time multiplied by absolute error (ITAE)

$$I = \int_0^{T_s (T_s \text{ or } \infty)} t |e(t)| dt$$

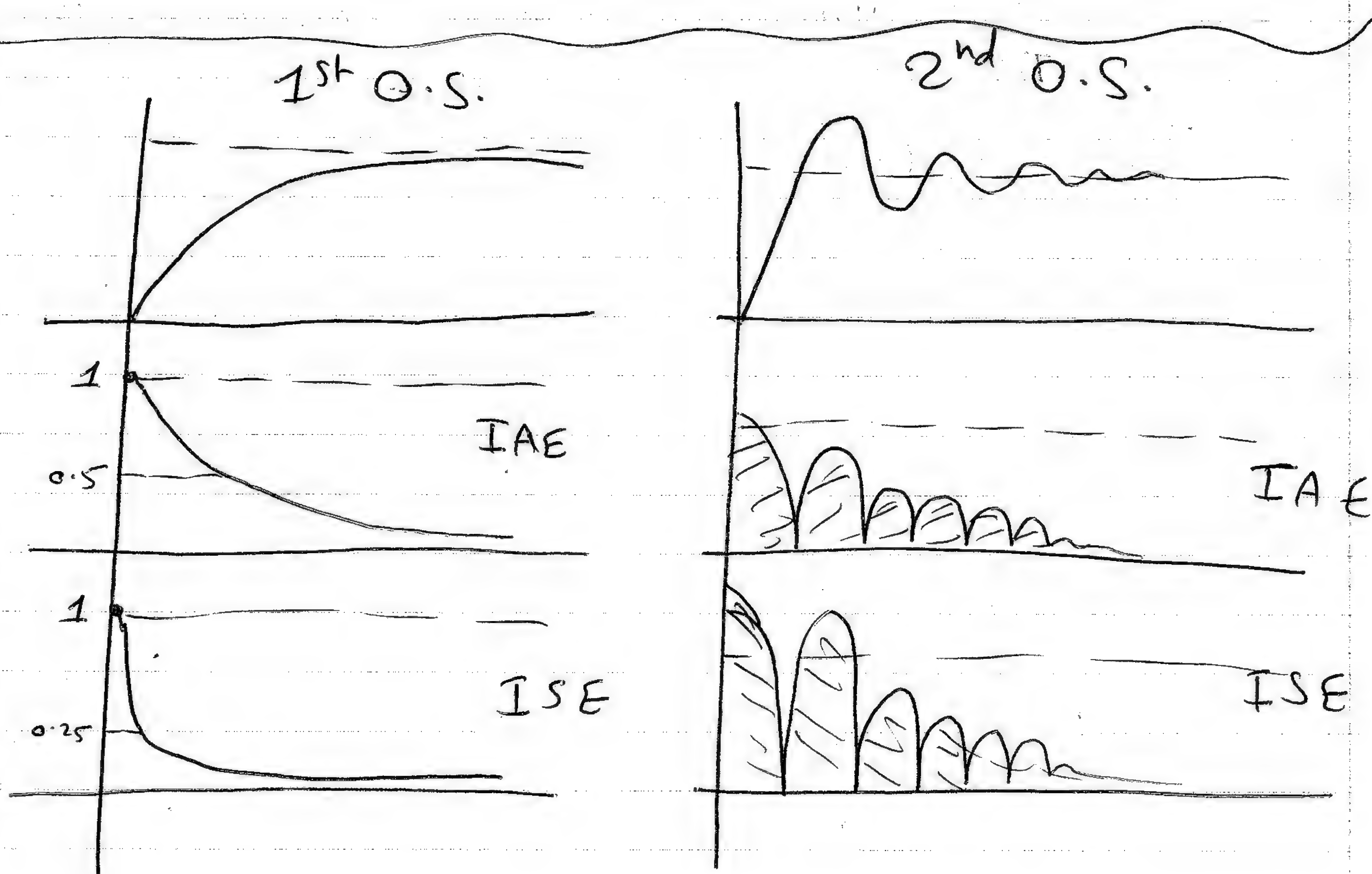
to reduce the contribution of ~~initial~~ Initial error,

$t = \infty$
 $e = 0$

(75)

4. Integral of time multiplied by square error (ITSE)

$$I = \int_0^{T_s} t e^2(t) dt$$

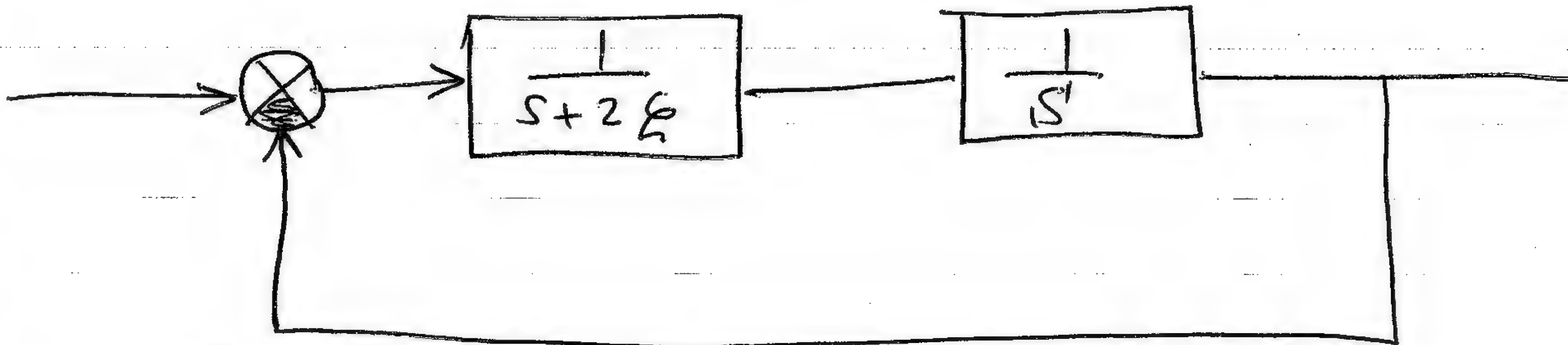


Example

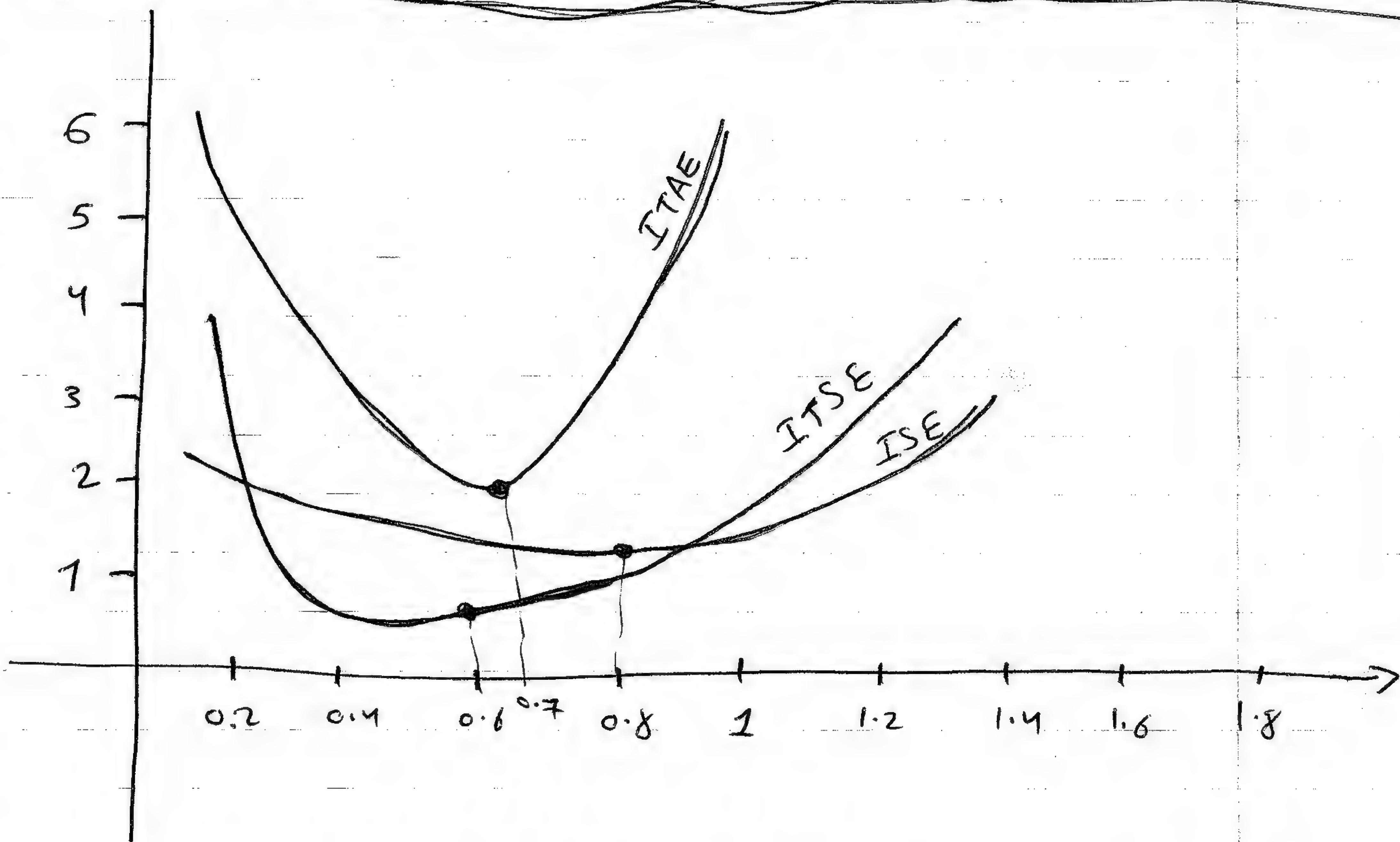
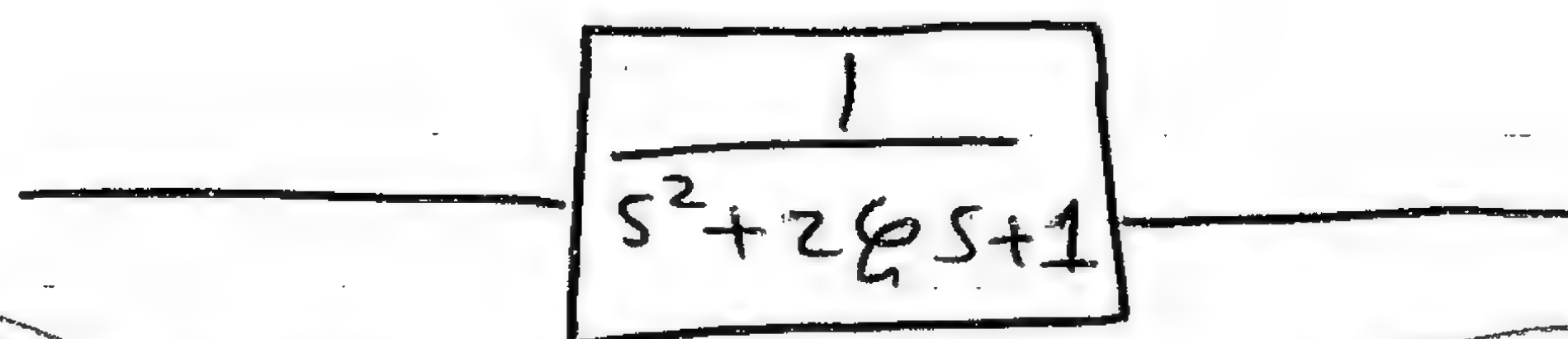
a single loop feedback control system is shown below where W_n is normalized ($W_n=1$).

Find the value of (ξ) so that the system is called optimum controlled.





|||



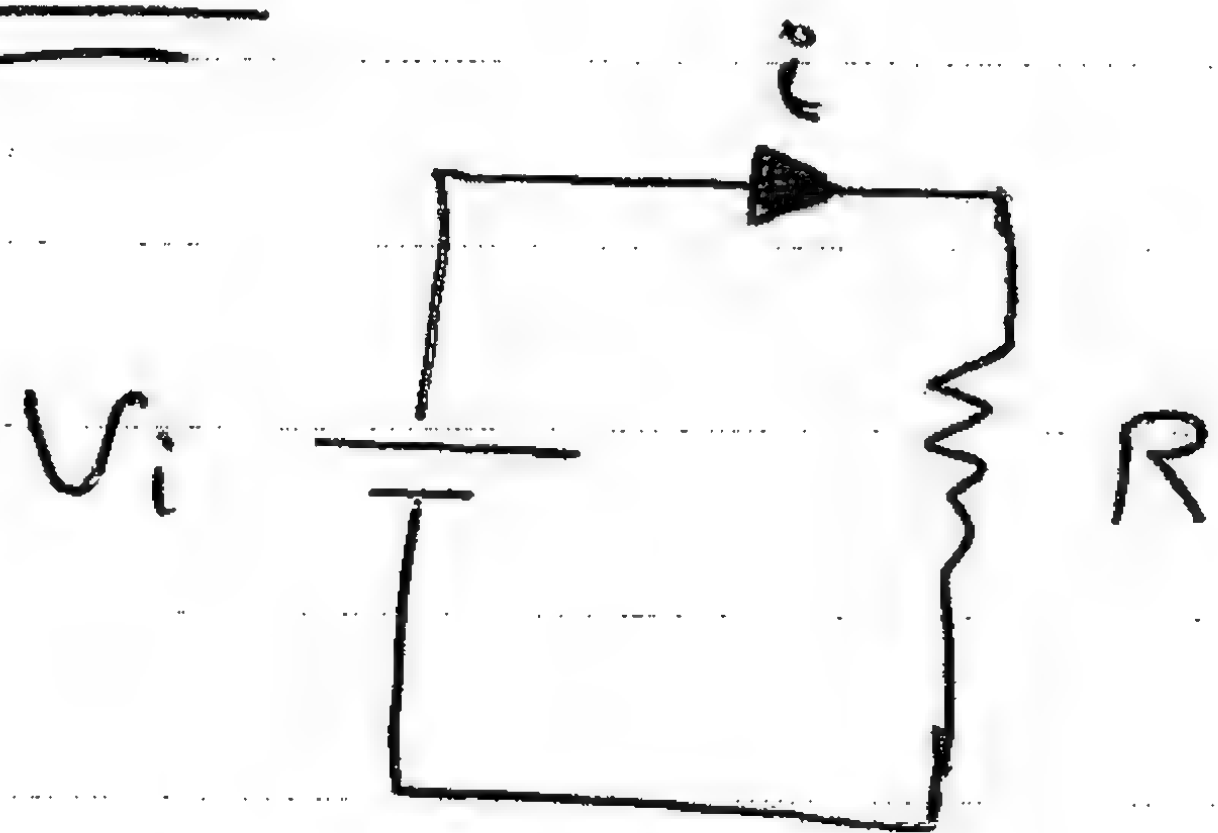
- ⊗ Optimal Value of ζ based on ITAE = $\boxed{0.7}$ ✓ ζ
- ⊗ optimal Value of ζ based on ITSE = $\boxed{0.6}$
- ⊗ optimal Value of ζ based on ISE = $\boxed{0.8}$

Control

Linear

Non-linear

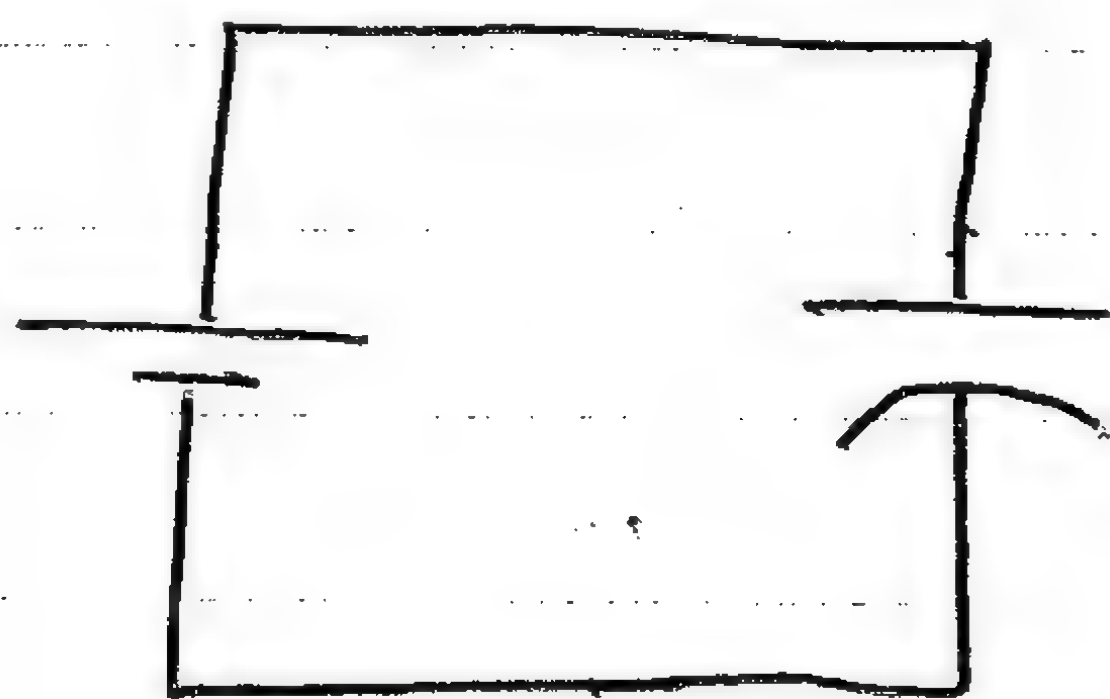
(Linear)



$$V = IR$$

$$V(s) = I(s) * R$$

(Linear)

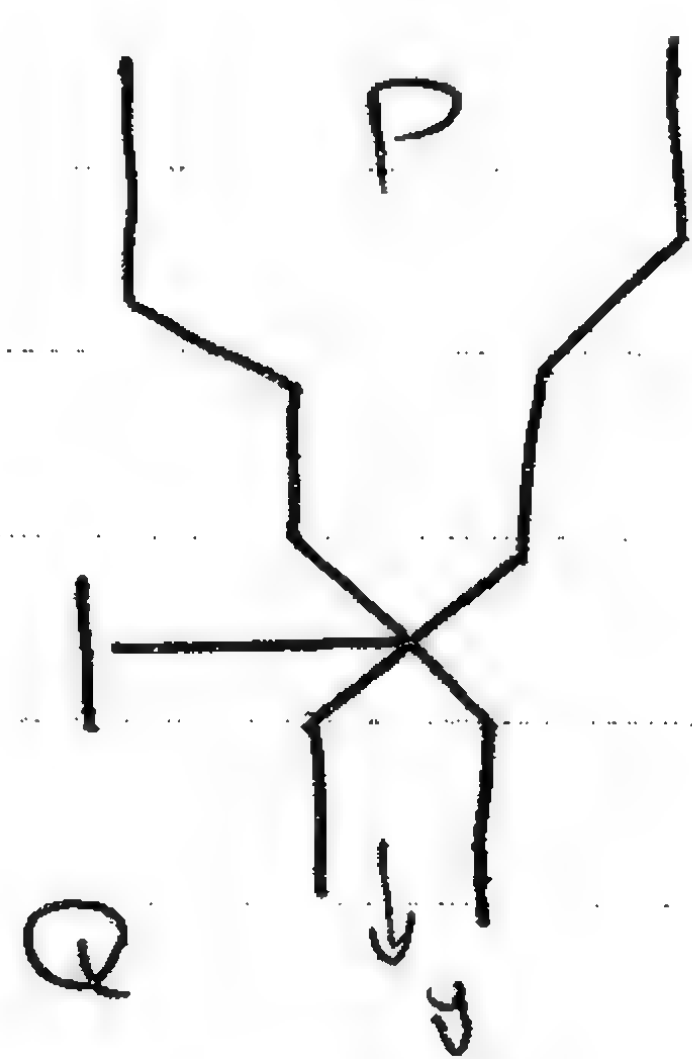


$$V = \frac{1}{C} \int i \, dt$$

$$V(s) = \frac{1}{C} \frac{I(s)}{s}$$

(Linear)

(Non-Linear)



$$Q = \frac{P}{R}$$

$$P = \rho gh$$

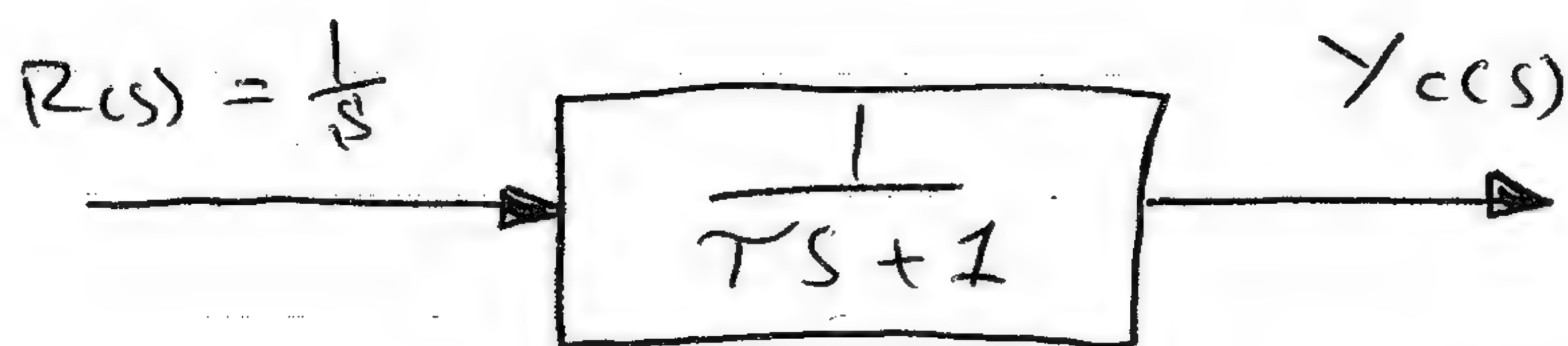
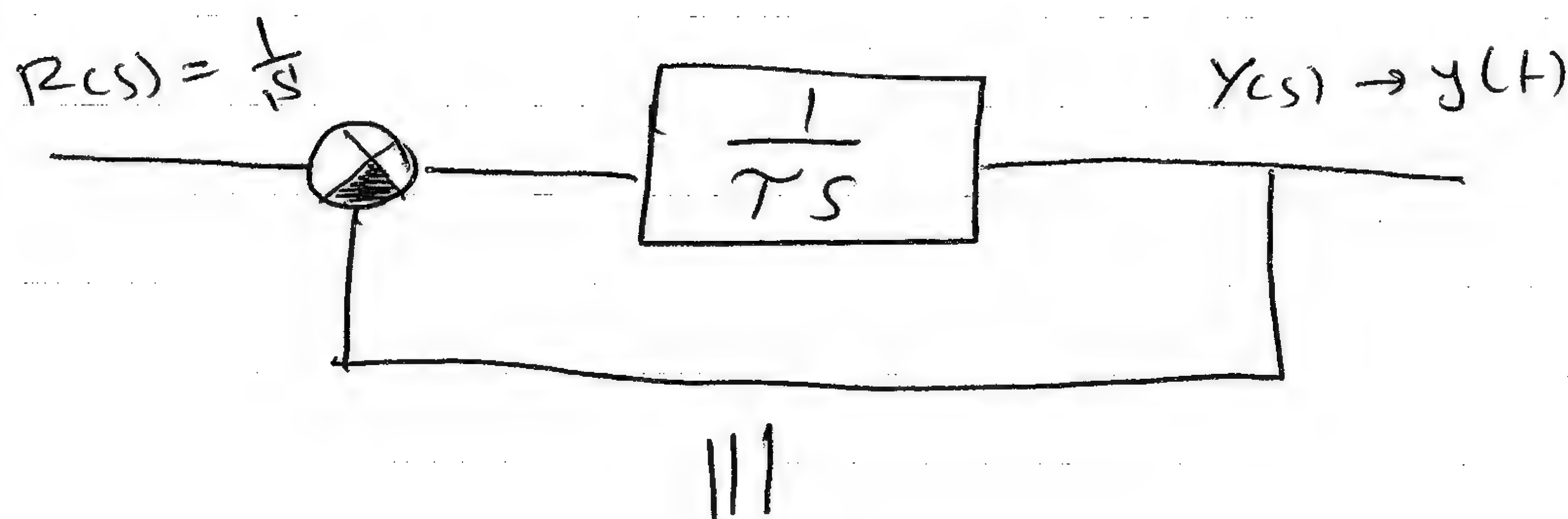
$$Q \propto \sqrt{\Delta P}$$

In Control 2, we study linear Control Systems only!

Continue :

Ex For the following system, find the performance Index based on IAE, ISE, ITAE, ITSE.

Note : Performance Index based on time domain.



$$y(t) = 1 - e^{-t/\tau}$$

$$e(t) = r(t) - y(t) = \boxed{e^{-t/\tau}}$$

$$\begin{aligned} \boxed{1.} \quad I_{IAE} &= \int_0^{\infty} |e^{-t/\tau}| dt = \int_0^{\infty} e^{-t/\tau} dt \\ &= \left[\frac{e^{-t/\tau}}{-1/\tau} \right]_0^{\infty} = -\tau e^{-t/\tau} \Big|_0^{\infty} \\ &= 0 - (-\tau) = \boxed{\tau} \end{aligned}$$

$$\boxed{2.} \quad I_{ISE} = \int_0^{\infty} (e^{-t/\tau})^2 dt = \int_0^{\infty} e^{-2t/\tau} dt$$

$$= \int_0^{\infty} e^{-t/\tau} dt = \boxed{\frac{\tau}{2}}$$

$$\boxed{3.} \quad I_{ITAE} = \int_0^{\infty} t |e^{-t/\tau}| dt$$

$$= \int_0^{\infty} t e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} - \int -\tau e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} + \tau \int e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} - \tau^2 e^{-t/\tau} \Big|_0^{\infty}$$

$$= [0 - 0] - [0 - \tau^2] = \boxed{\tau^2}$$

$$\boxed{4.} \quad I_{ITSE} = \int_0^{\infty} t (e^{-t/\tau})^2 dt = \int_0^{\infty} t e^{-2t/\tau} dt$$

Suppose $L = \tau/2$

$$\therefore \int_0^{\infty} t e^{-t/L} dt \quad \left(\begin{array}{l} \uparrow \\ \text{نفس حل القسم الثالث أعلاه} \end{array} \right)$$

$$\therefore \int_0^{\infty} t e^{-t/L} dt = \boxed{\tau^2} L^2$$

but $L = \tau/2$

$$\therefore \text{Answer} = \boxed{\frac{\tau^2}{4}}$$

Back to Sensitivity

There is a mathematical Method to compute \sqrt{x} .

Ex We need to find $\sqrt{5}$

Solution

$$y = \sqrt{x}$$

$$\frac{dy}{dx} = \frac{1}{2\sqrt{x}}$$

$$\frac{\Delta y}{\Delta x} = \frac{1}{2\sqrt{x_0}}$$

$$\Delta y = \frac{1}{2\sqrt{x_0}} * \Delta x = \frac{1}{2\sqrt{4}} * 1 = \frac{1}{4} * 1 = \frac{1}{4}$$

$$= \boxed{0.25}$$

$$\therefore \sqrt{5} = y + \Delta y = 2 + 0.25 = \boxed{2.25}$$

$$y_0 = \sqrt{x_0}$$

$$2 = \sqrt{4}$$

$$y_0 + \Delta y = \sqrt{5}$$

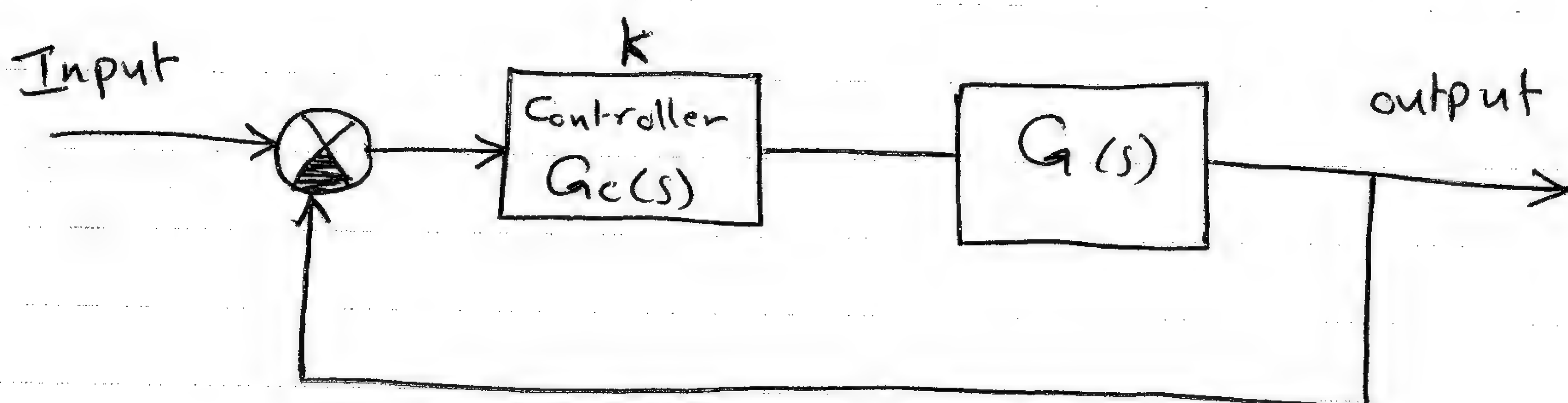
$$2 + \Delta y = \sqrt{5}$$

$$dx = 1 \approx \Delta x$$

System Sensitivity : is the ratio of change in the System transfer function to the change of a process transfer function (or parameter) for a small incremental change.

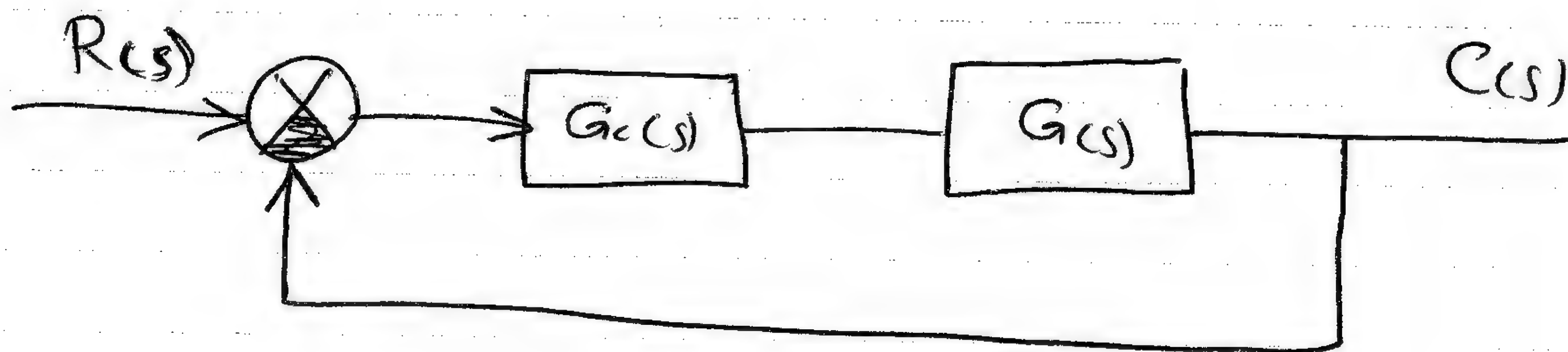
$$T(s) = \frac{Y(s)}{R(s)}$$

$$S_G^T = \frac{dT/T}{dG/G} = \frac{d \ln T}{d \ln G}$$



$$\therefore S_G^T = \frac{dT/T}{dG/G} = \frac{d \ln T}{d \ln G} = \frac{dT}{dG} \cdot \frac{G}{T}$$

Ex For the following system, find the Sensitivity of the system to process.



$$T(s) = \frac{G_c G}{1 + G_c G}$$

⇒

$$S_G^T = \frac{dT}{dG} * \frac{G}{T}$$

$$\Rightarrow \frac{dT}{dG} = \frac{(1+G_c G) G_c - G_c G G_c}{(1+G_c G)^2}$$

~~$$\frac{G_c}{(1+G_c G)^2}$$~~

$$= \frac{G_c + G_c^2/G - G_c^2/G}{(1+G_c G)^2}$$

$$= \boxed{\frac{G_c}{(1+G_c G)^2}}$$

~~$$\frac{dT}{dG}$$~~

$$S_G^T = \frac{dT}{dG} * \frac{G}{T} = \frac{G_c}{(1+G_c G)^2} * \frac{G}{\frac{G_c G}{1+G_c G}}$$

$$= \frac{1+G_c G}{(1+G_c G)^2} = \boxed{\frac{1}{1+G_c G}}$$

* For the upper system, find the sensitivity of the system to feed back.

$$S_H^T = \frac{dT}{dH} * \frac{H}{T}$$

$$T(s) = \frac{G_c G}{1 + G_c G H}$$

$$\frac{dT}{dH} = \frac{(1 + G_c G H)(0) - (G_c G)(G_c G)}{(1 + G_c G H)^2}$$

$$= \frac{-G_c^2 G^2}{(1 + G_c G H)^2}$$

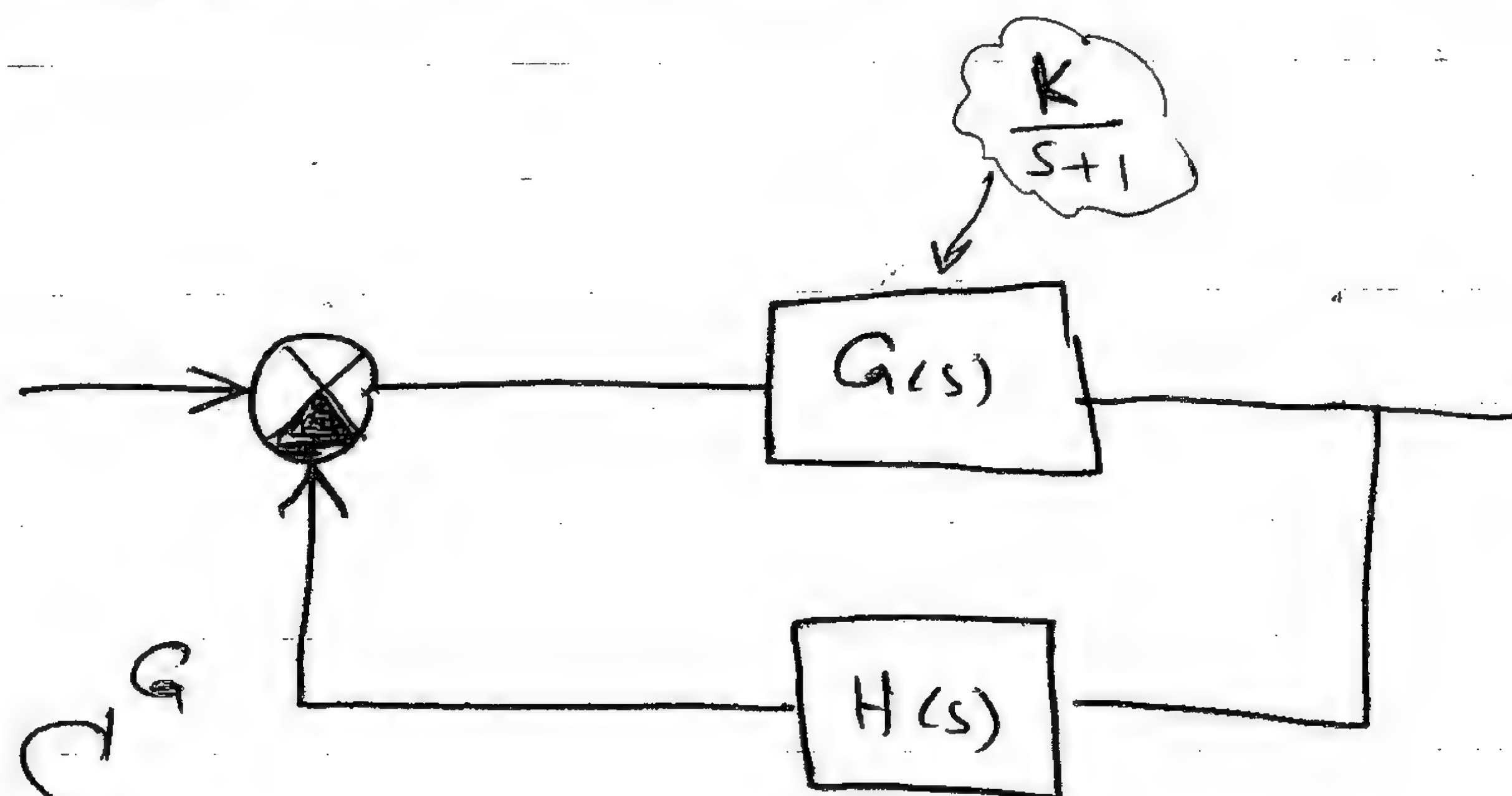
$$\therefore S_H^T = \frac{dT}{dH} * \frac{H}{T} = \frac{-G_c^2 G^2}{(1 + G_c G H)^2} * \frac{H}{\frac{G_c G}{1 + G_c G H}}$$

$$= \boxed{\frac{-G_c G H}{1 + G_c G H}}$$

Chain Rule

$$S_{\alpha}^T = S_G^T * S_{\alpha}^G$$

for example:



$$S_K^T = S_G^T * S_K^G$$

$$T.F. = \frac{G}{1+GH}$$

$$\textcircled{1} S_G^T = \frac{dT}{dG} * \frac{G}{T} = \frac{1+GH - GH}{(1+GH)^2} * \frac{G}{\frac{G}{1+GH}} = \boxed{\frac{1}{1+GH}}$$

$$\textcircled{2} S_K^G = \frac{dG}{dk} * \frac{k}{G}$$

$$G = \frac{k}{s+1}$$

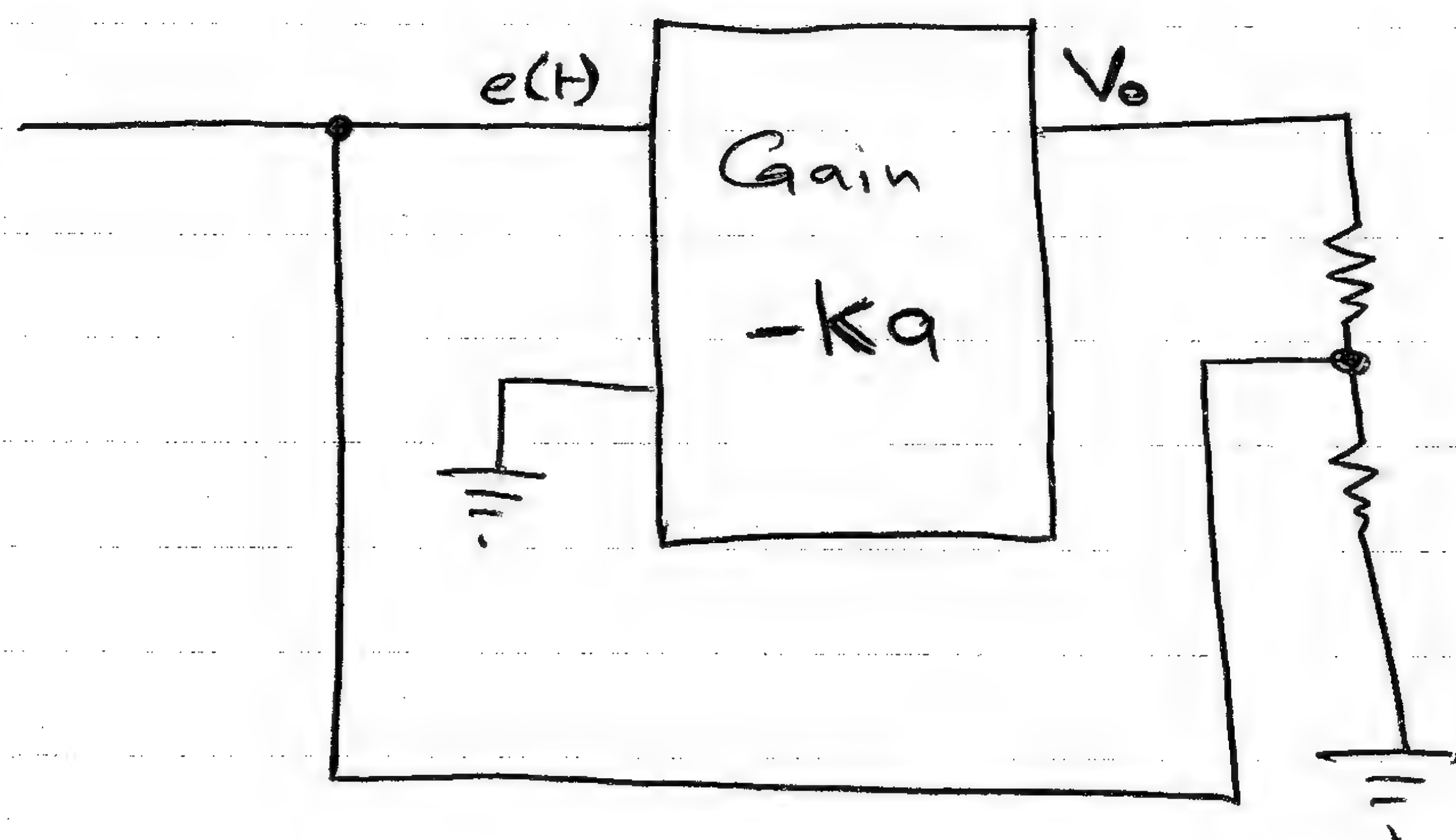
$$\therefore S_K^G = \frac{dG}{dk} * \frac{k}{G} = \frac{1}{s+1} * \frac{k}{\frac{k}{s+1}} = 1 * 1 = \boxed{1}$$

$$\Rightarrow \therefore S_K^T = S_G^T * S_K^G = \frac{1}{1+GH} * 1 = \boxed{\frac{1}{1+GH}}$$

Example :- Feed back Amplifier

Find the sensitivity of the system to $|k_a|$

$\therefore \frac{d|k_a|}{|k_a|}$
 $S_{k_a}^T$



$$\beta = \frac{R_2}{R_1 + R_2}$$

$$e(t) = V_{in} + \frac{V_o * R_2}{R_1 + R_2} \quad \text{--- (1)}$$

$$V_o = e(t) * -k_a \quad \text{--- (2)}$$

$$e(t) = V_{in} + \frac{V_o * R_2}{R_1 + R_2} ; \quad \text{divide } \frac{V_o * R_2}{R_1 + R_2} \text{ on } R_1$$

$$\therefore e(t) = V_{in} + \frac{V_o \beta}{1 + \beta} \quad \text{--- (1) } * *$$

$$V_o = e(t) * -k_a \quad \text{--- (2)}$$

From (1) and (2) :-

$$V_o = \left[V_{in} + \frac{\beta}{\beta + 1} V_o \right] * -k_a$$

$$\Rightarrow V_o = -k_a V_{in} - \frac{\beta}{\beta+1} k_a V_o$$

$$\Rightarrow V_o + \frac{\beta}{\beta+1} k_a V_o = -k_a V_{in}$$

$$\Rightarrow \boxed{\frac{V_o}{V_{in}} = \frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}}$$

$$\therefore T = \frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}$$

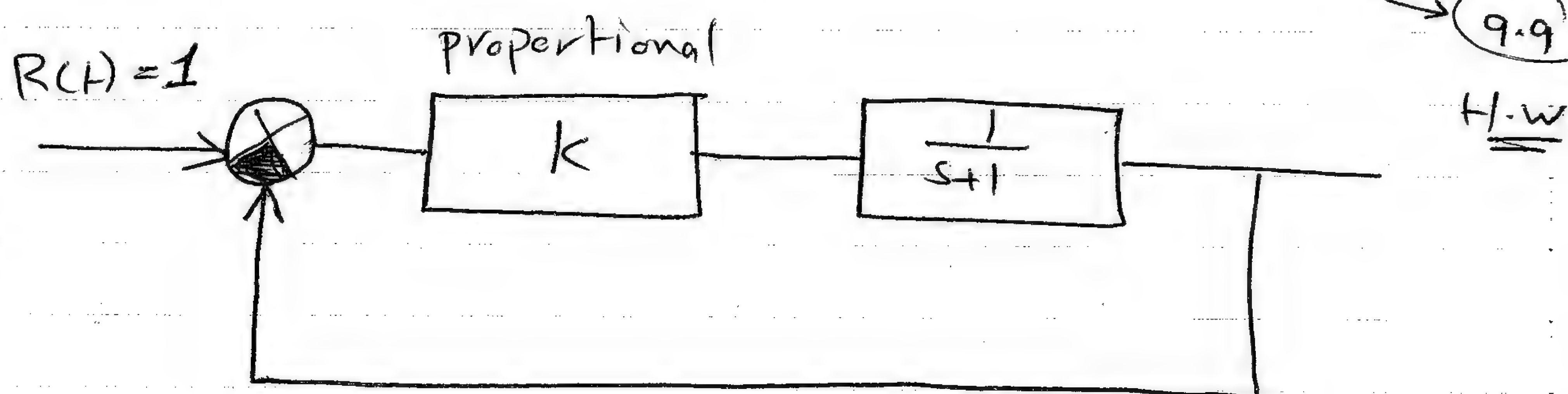
$$S_{k_a}^T = \frac{dT}{dk_a} * \frac{k_a}{T}$$

$$\frac{dT}{dk_a} = \frac{\left(1 + \frac{\beta}{\beta+1} k_a\right)(-1) - (-k_a)\left(\frac{\beta}{\beta+1}\right)}{\left(1 + \frac{\beta}{\beta+1} k_a\right)^2}$$

$$\therefore S_{k_a}^T = \frac{\left(1 + \frac{\beta}{\beta+1} k_a\right)(-1) + (k_a)\left(\frac{\beta}{\beta+1}\right)}{\left(1 + \frac{\beta}{\beta+1} k_a\right)^2} * \frac{k_a}{\frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}}$$

$$\approx \boxed{\frac{1}{1 + \frac{\beta}{\beta+1} k_a}}$$

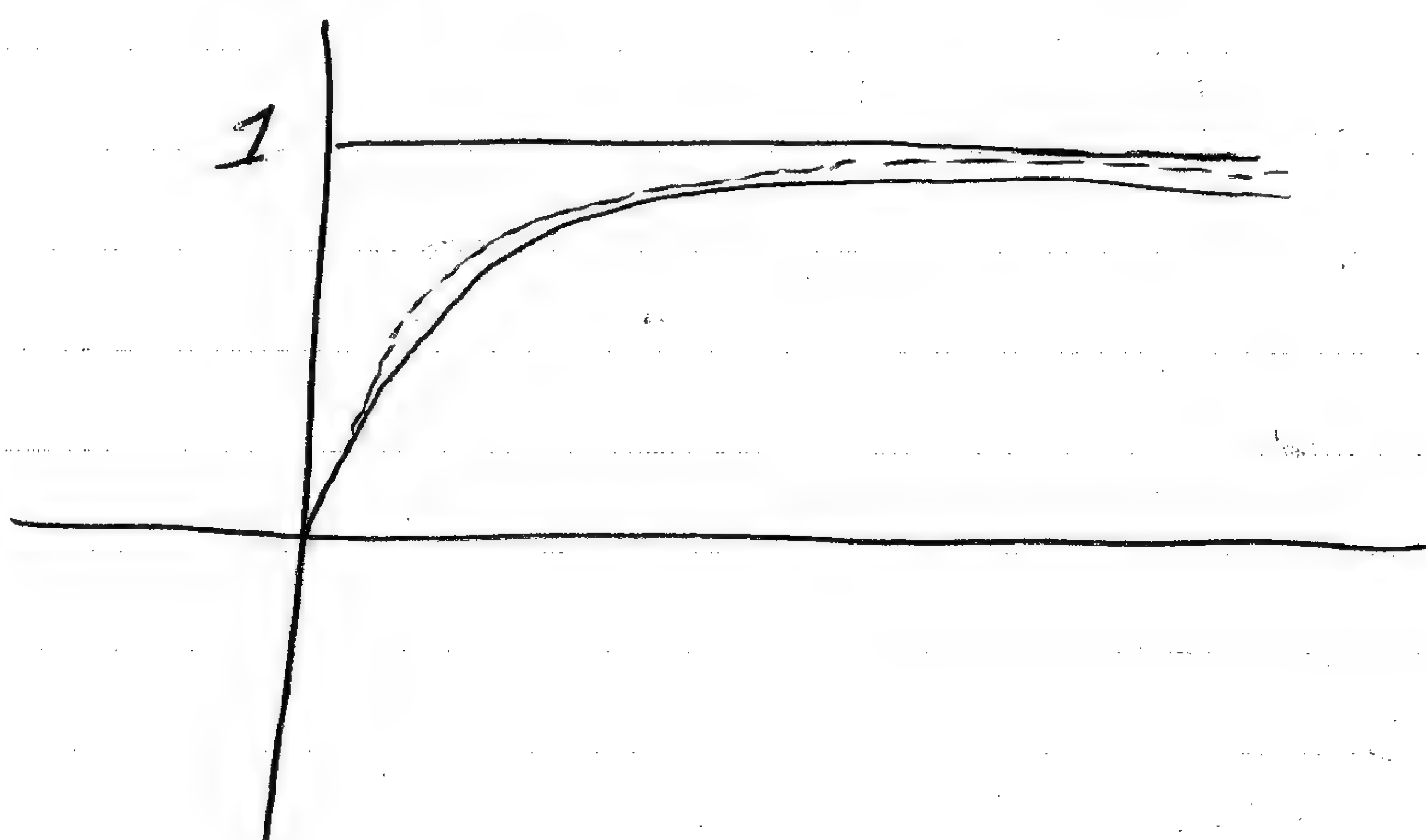
Ex :- For the following example, find the response of the system as k varies from 10 to 11



$$Y_{ss} = \frac{k}{1+k} R$$

$$Y_{ss} \Big|_{k=10} = \frac{10}{1+10} * 1 = \frac{10}{11} = \boxed{0.909}$$

$$Y_{ss} \Big|_{k=11} = \frac{11}{1+11} * 1 = \frac{11}{12} = \boxed{0.916}$$



$$S_k^T = \frac{dT}{dk} * \frac{k}{T}$$

$$T(s) = \frac{kG}{1+kG}$$

$$\therefore S_k^T \approx \frac{dT}{dk} * \frac{k}{T}$$

$$= \frac{(1+kG)G - kG * G}{(1+kG)^2} * \frac{k}{\frac{kG}{1+kG}}$$

$$= \boxed{\frac{-1}{1+kG}}$$

$$= \frac{1}{1 + \frac{k}{s+1}}$$

$$\boxed{\frac{s+1}{s+1+k}}$$

~~$$\frac{1}{1+k}$$~~

⊗ at static response $\Rightarrow S=0$

$$S_k^T = \frac{0+1}{0+1+k} = \boxed{\frac{1}{1+k}}$$

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

12/17 سنه (إكمال حل المسألة الخاصة بالحاضر الخاصة)

$$S_G^T = \frac{\frac{\Delta T}{T}}{\frac{\Delta G}{G}} \Rightarrow \frac{\Delta T}{T} = S * \frac{\Delta G}{G}$$

$$Y = T * X$$

$$Y_{\text{new}} = (T + \Delta T) X$$

$$Y_n = Y + \Delta T X$$

$$= X T \left(1 + \frac{\Delta T}{T} \right)$$

$$= Y \left(1 + \frac{\Delta T}{T} \right)$$

Back To the previous Question (Page 88) :-

$$S_K^T = \frac{1}{1+k}$$

$$\frac{\Delta T}{T} = S_K^T * \frac{\Delta k}{k}$$

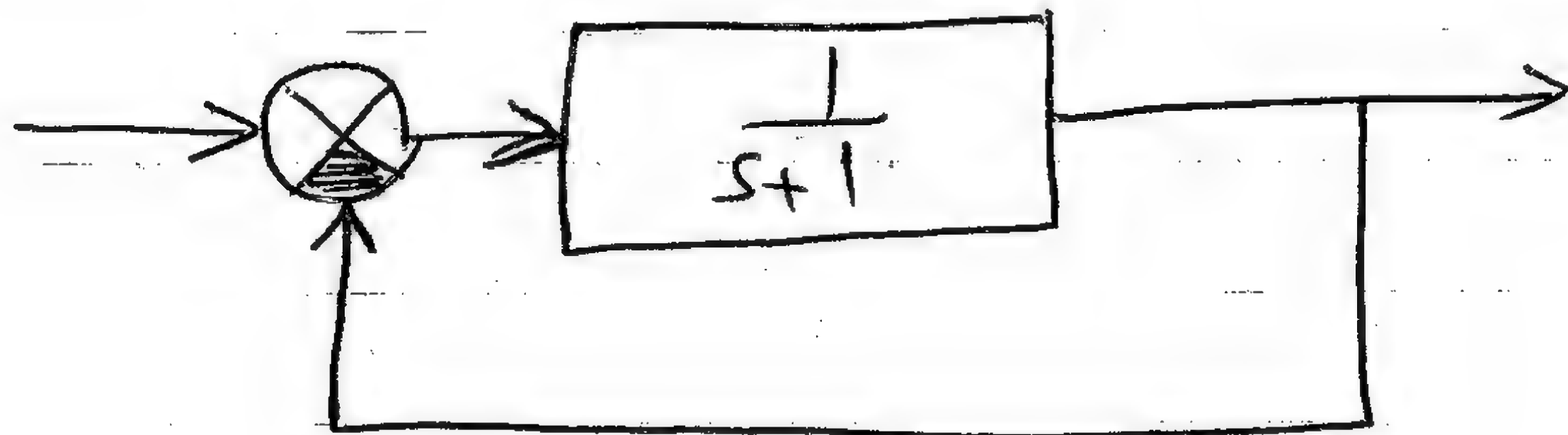
$$= \cancel{\frac{1}{1+10}} * \frac{1}{10} = \frac{1}{11} * \frac{1}{10} = \boxed{\frac{1}{110}}$$

$$Y_n = Y \left(1 + \frac{1}{110} \right)$$

$$= 0.909 \left(1 + \frac{1}{110} \right) = \boxed{0.917}$$

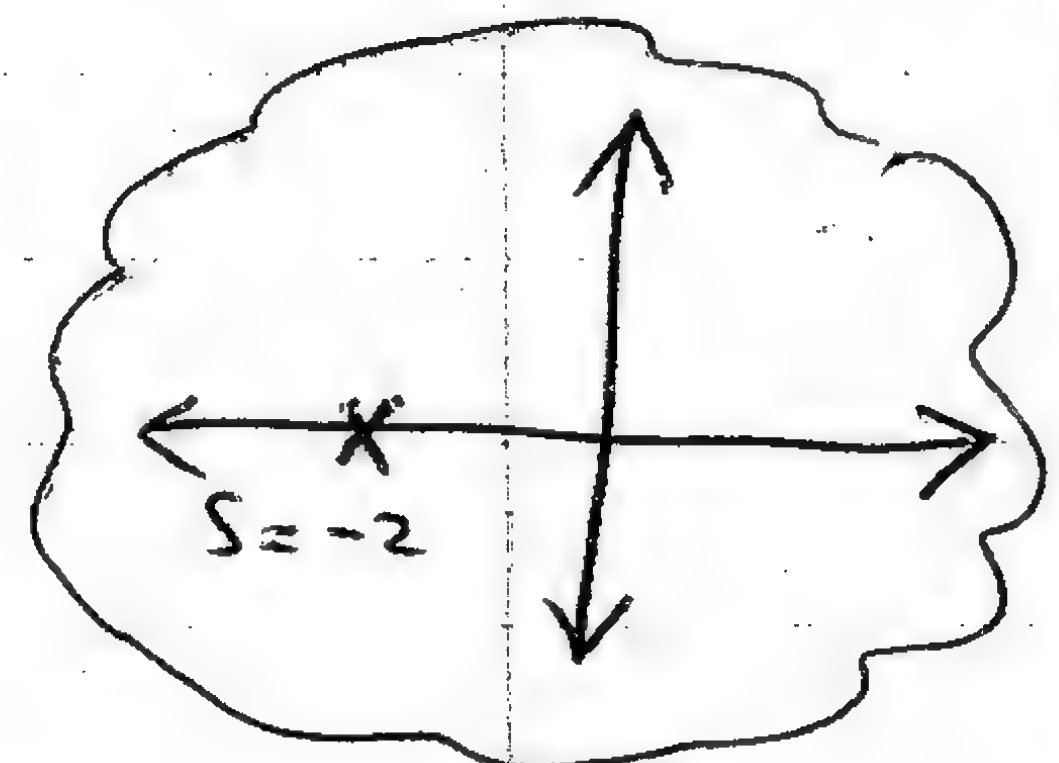
Root Loci

Ex

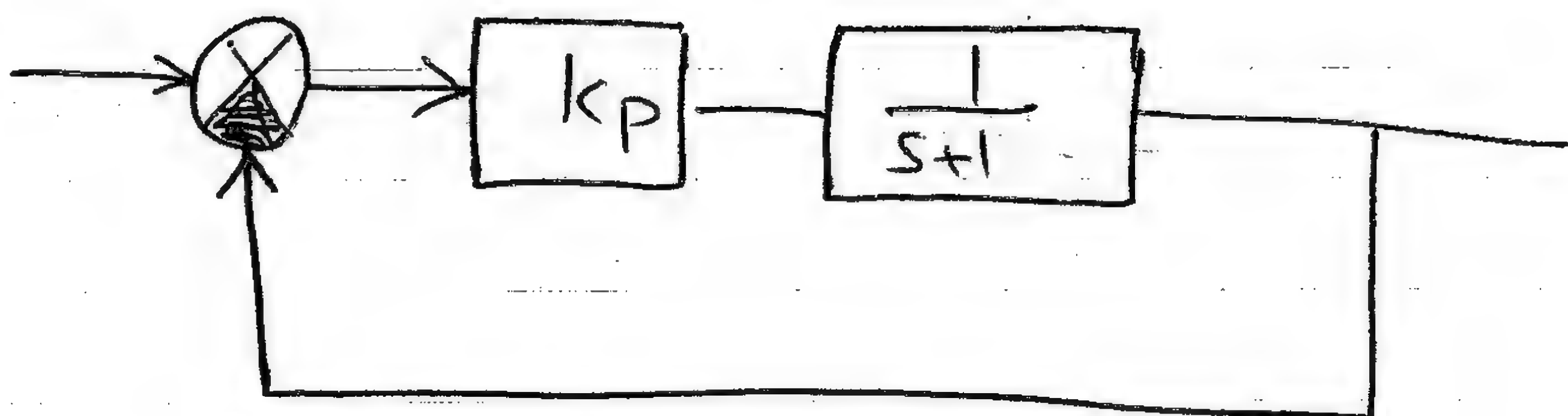


$$T.F. = \frac{1}{s+2}$$

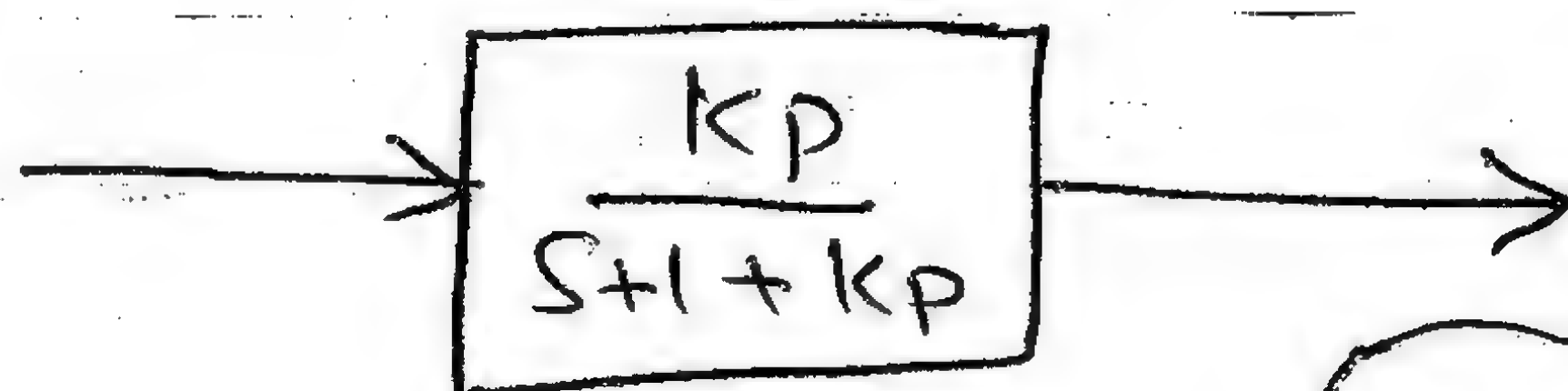
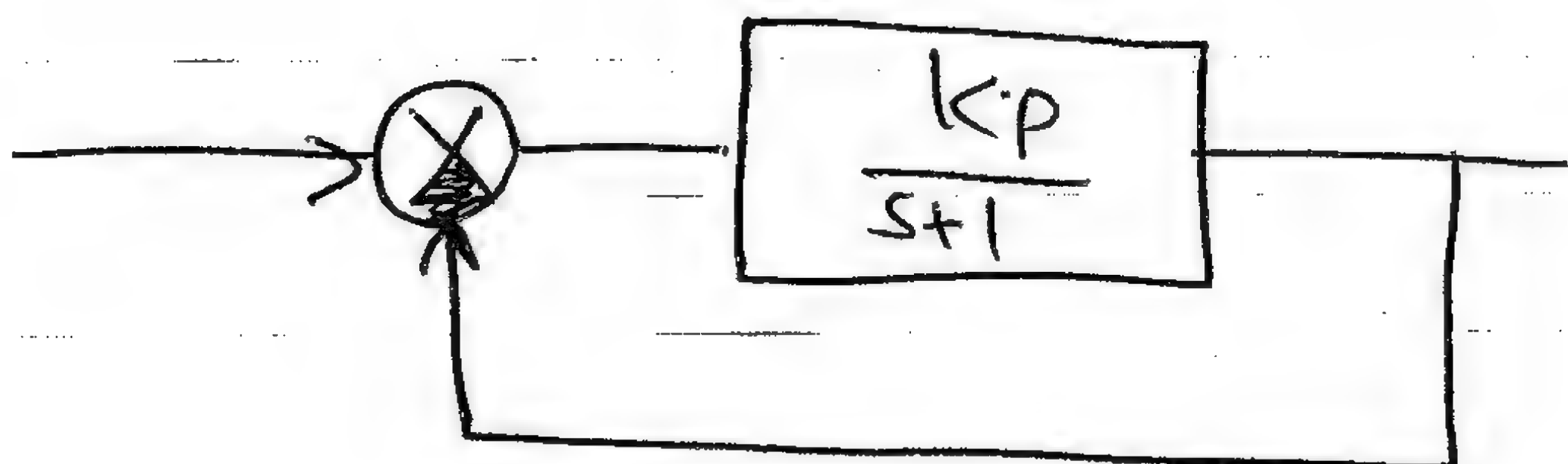
$$q(s) = s+2=0 \Rightarrow \boxed{s=-2} \quad \therefore \text{Stable}$$



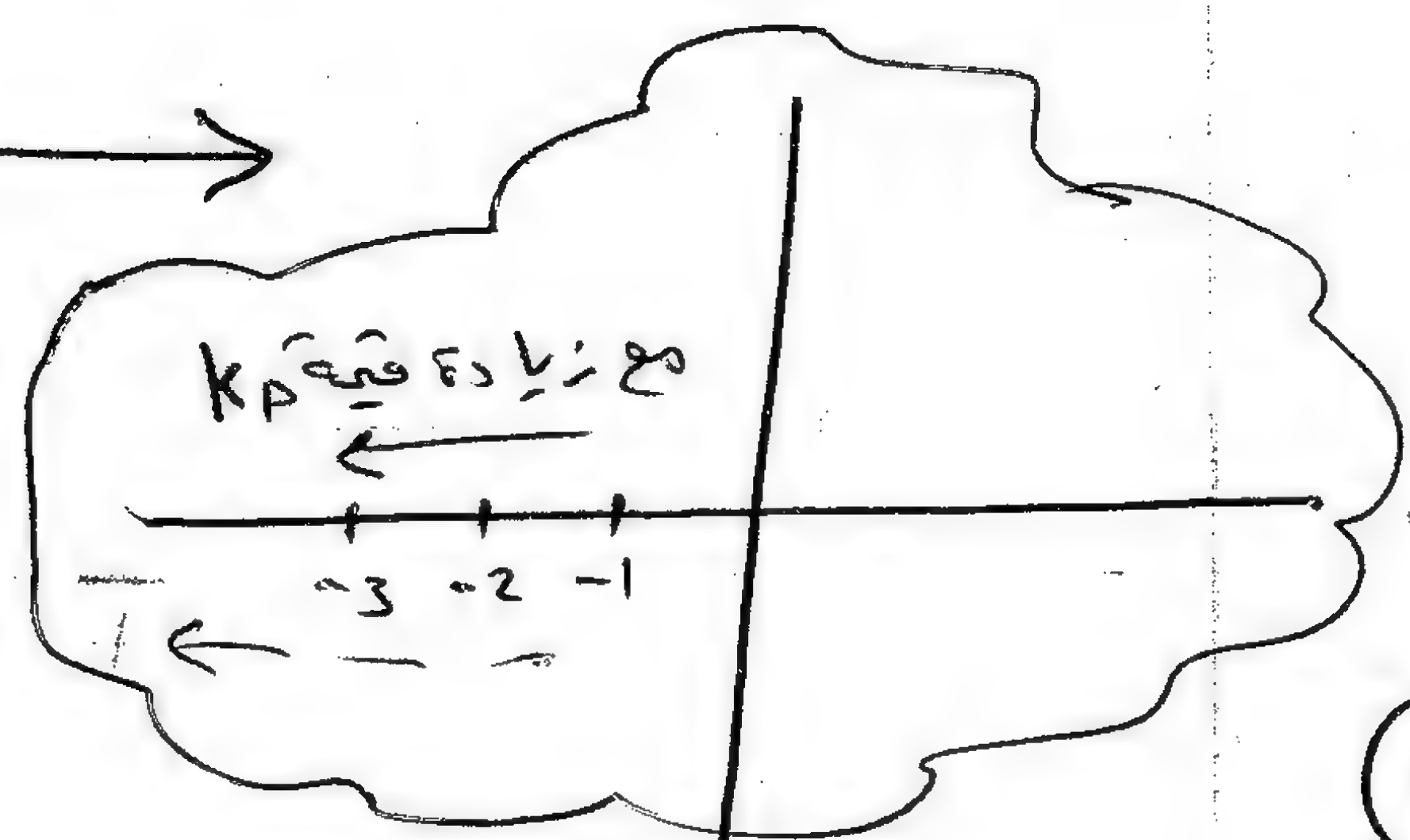
Ex



$$\boxed{k_p = 0 \rightarrow \infty}$$

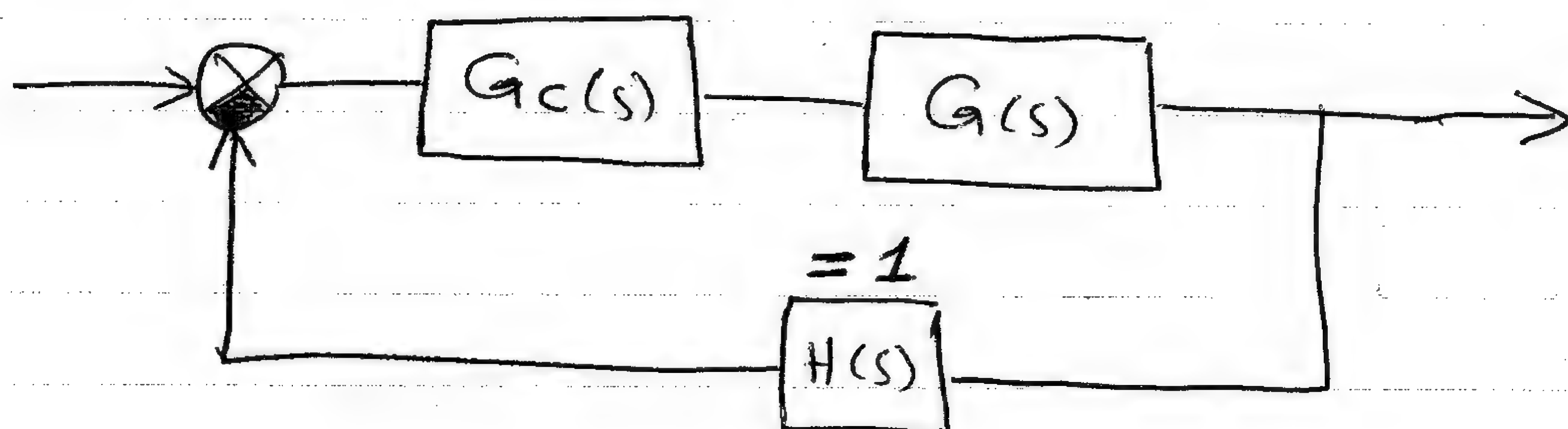


$$\boxed{s = -1 - k_p}$$



Root Loci :- it determines how the roots of characteristic equation move around the s -plane as we change one parameter from $0 \rightarrow \infty$ by a graphical Method.

⊛ This method was introduced by Evan in 1948



$$T(s) = \frac{G_c(s) G(s)}{1 + G_c(s) G(s) H(s)}$$

$$Q(s) = 1 + G_c(s) G(s) H(s)$$

$$Q(s) = 1 + K G(s) = 0$$

$$\Rightarrow K G(s) = -1$$

$$\Rightarrow K G(s) = -1 + j0 = |K G(s)| \angle K G(s) = -1 + j0$$

$$|K G(s)| = 1$$

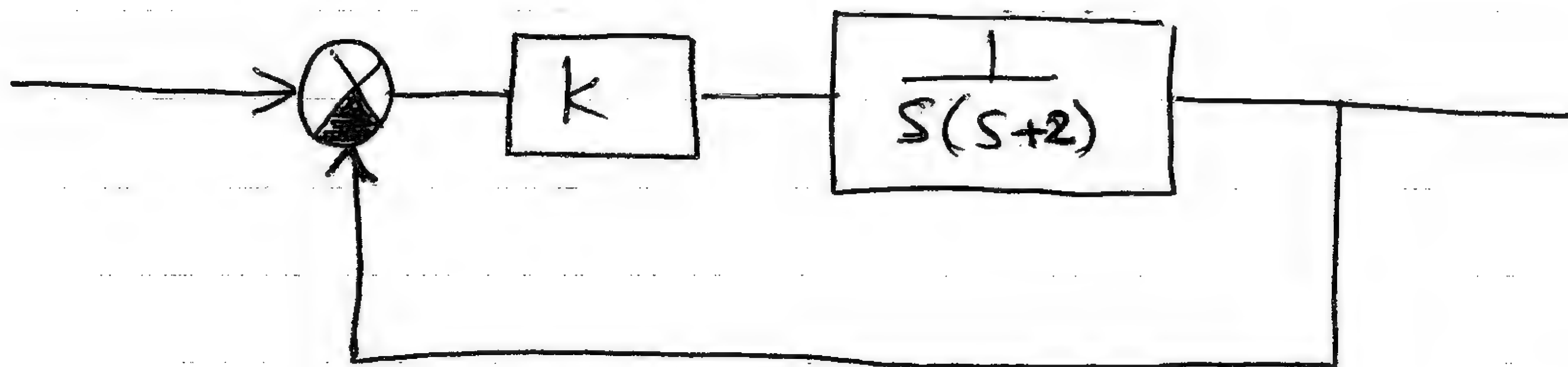
$$\angle K G(s) = 180^\circ \mp k \times 360^\circ$$

$$k = 1, 2, 3, 4, \dots$$

⇒ We prefer to use angle -180°

⊕ The root locus is the path of the roots of the ch. equ. traced out in s -plane as system parameter is changed from zero \rightarrow infinity.

Ex Find the root locus of the following system.



$$T(s) = \frac{K}{s^2 + 2s + K}$$

as K varies from zero $\rightarrow \infty$

$$\begin{aligned} q(s) &= s^2 + 2s + K = 0 \\ &= s^2 + 2\zeta\omega_n s + \omega_n^2 = 0 \end{aligned}$$

$$s_{1,2} = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

⊕ We want to sketch the function [نقشه]

we will take some points :-

① $K=0 \Rightarrow q(s) = s^2 + 2s = 0 \Rightarrow s(s+2) \Rightarrow s_{1,2} = \underline{\underline{0, -2}}$

② $K=0.5 \Rightarrow q(s) = s^2 + 2s + 0.5 = 0$

$$\Rightarrow s_{1,2} = \frac{-2 \pm \sqrt{4-2}}{2} = -1 \pm \frac{1}{\sqrt{2}} = \boxed{-1 \pm 0.7}$$

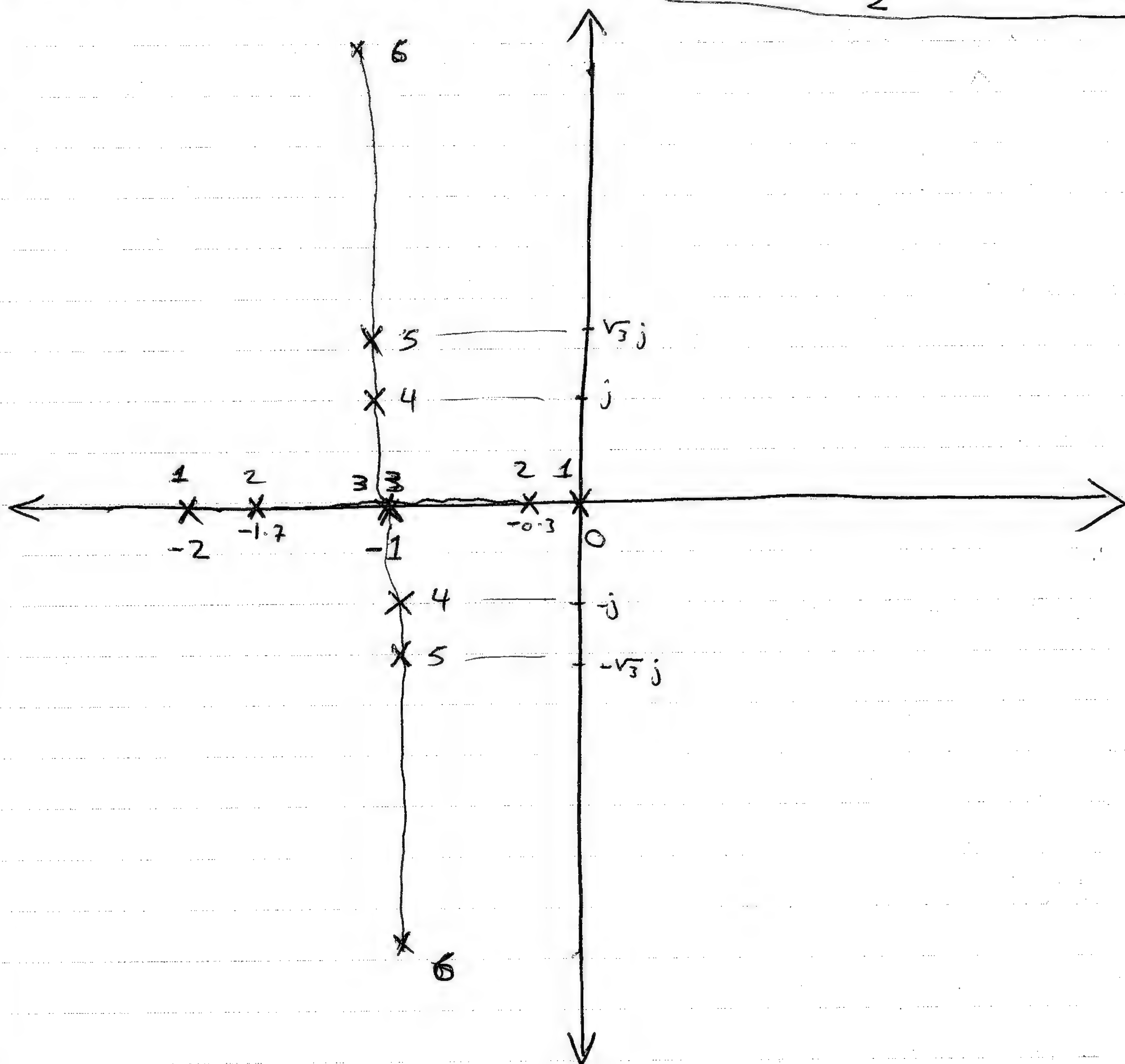
$$\Rightarrow -1 + 0.7 = \boxed{-0.3} \text{ and } -1 - 0.7 = \boxed{-1.7}$$

$$\textcircled{3} \quad k=1 \Rightarrow q(s) = s^2 + 2s + 1 = 0 \Rightarrow s_{1,2} = \boxed{-1}$$

$$\textcircled{4} \quad k=2 \Rightarrow q(s) = s^2 + 2s + 2 = 0 \Rightarrow s_{1,2} = \boxed{-1 \pm j1}$$

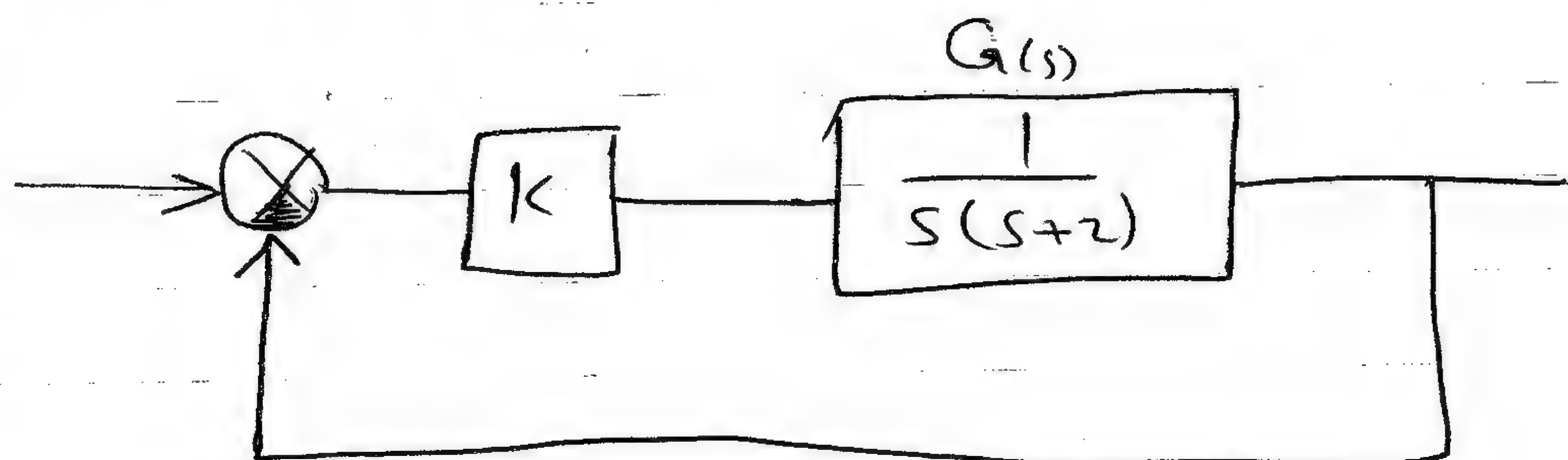
$$\textcircled{5} \quad k=4 \Rightarrow q(s) = s^2 + 2s + 4 = 0 \Rightarrow s_{1,2} = \boxed{-1 \pm j\sqrt{3}}$$

$$\textcircled{6} \quad k=\infty \Rightarrow q(s) = s^2 + 2s + \infty = 0 \Rightarrow s_{1,2} = \frac{-2 \pm \sqrt{4-\infty}}{2} = \boxed{-1 \pm j\infty}$$



12/12 2021

Back to previous example :-



$$T(s) = \frac{\frac{k}{s(s+2)}}{\frac{k}{s(s+2)} + 1}$$

$$KG(s) + 1 = 0$$

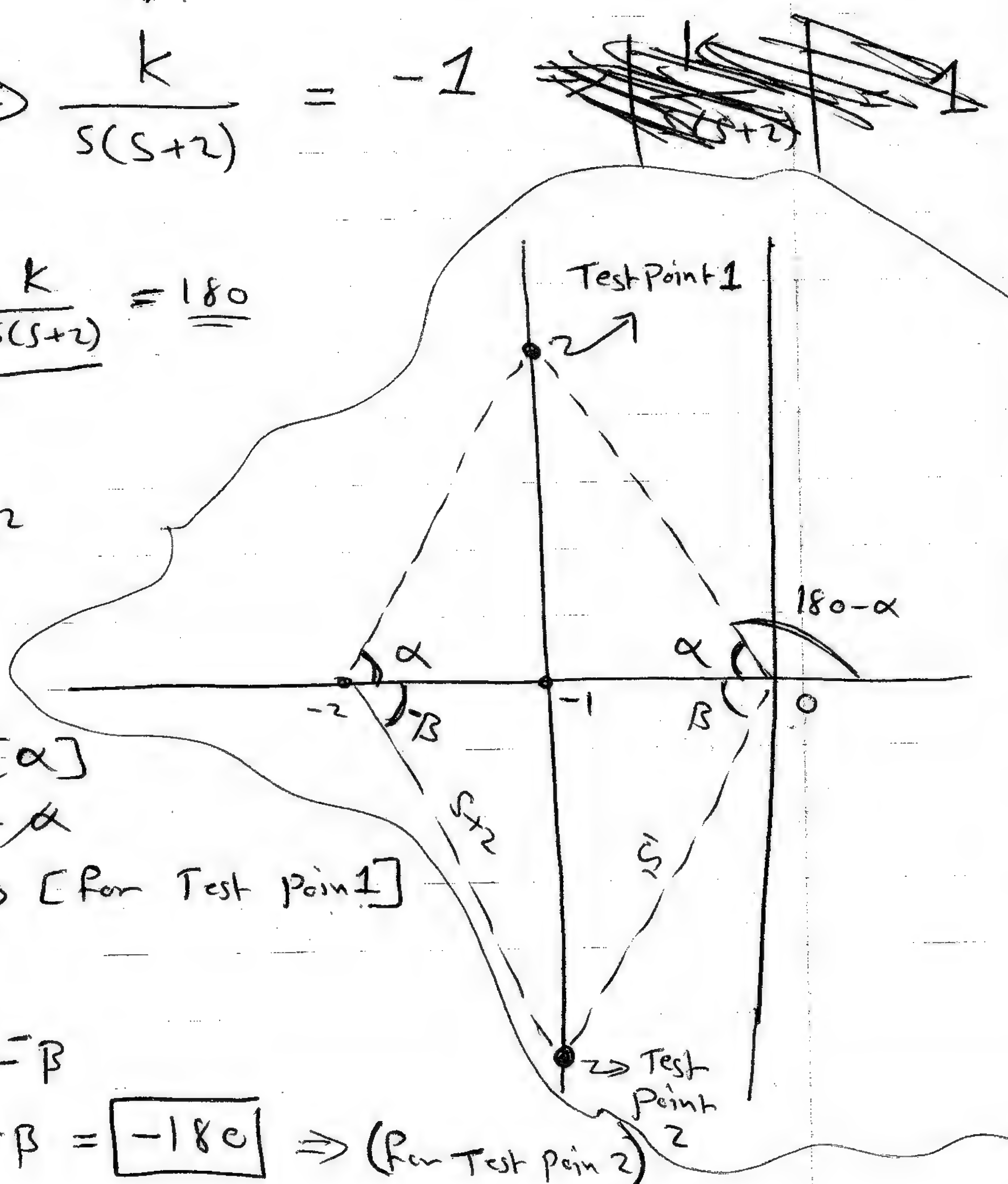
$$\frac{k}{s(s+2)} + 1 = 0 \Rightarrow \frac{k}{s(s+2)} = -1$$

$$\Rightarrow \left| \frac{k}{s(s+2)} \right| = 1 \quad \angle \frac{k}{s(s+2)} = \underline{180}$$

$$\boxed{180} = 0 - \angle s - \angle s+2$$

$$\begin{aligned} \text{angle} &= 0 - [180 - \alpha] - [\alpha] \\ &= 0 - 180 + \alpha - \alpha \\ &= \boxed{-180} \Rightarrow [\text{For Test point 1}] \end{aligned}$$

$$\begin{aligned} \text{angle} &= 0 - [180 + \beta] - \beta \\ &= -180 - \beta + \beta = \boxed{-180} \Rightarrow [\text{For Test point 2}] \end{aligned}$$



$$\left| \frac{k}{s(s+2)} \right| = 1 \Rightarrow \frac{|k|}{|s| |s+2|} = 1 \Rightarrow \frac{k}{|s| |s+2|} = 1$$

① at $k=1$ (Test Point 1) (TP1)

$$\Rightarrow \frac{1}{|1| |1|} = 1$$

② at TP2 $k=2$

$$\frac{k}{|s| |s+2|} = 1$$

$$|s| = \sqrt{1^2 + 1^2} = \sqrt{2}$$

$$|s+2| = \sqrt{1^2 + 1^2} = \sqrt{2}$$

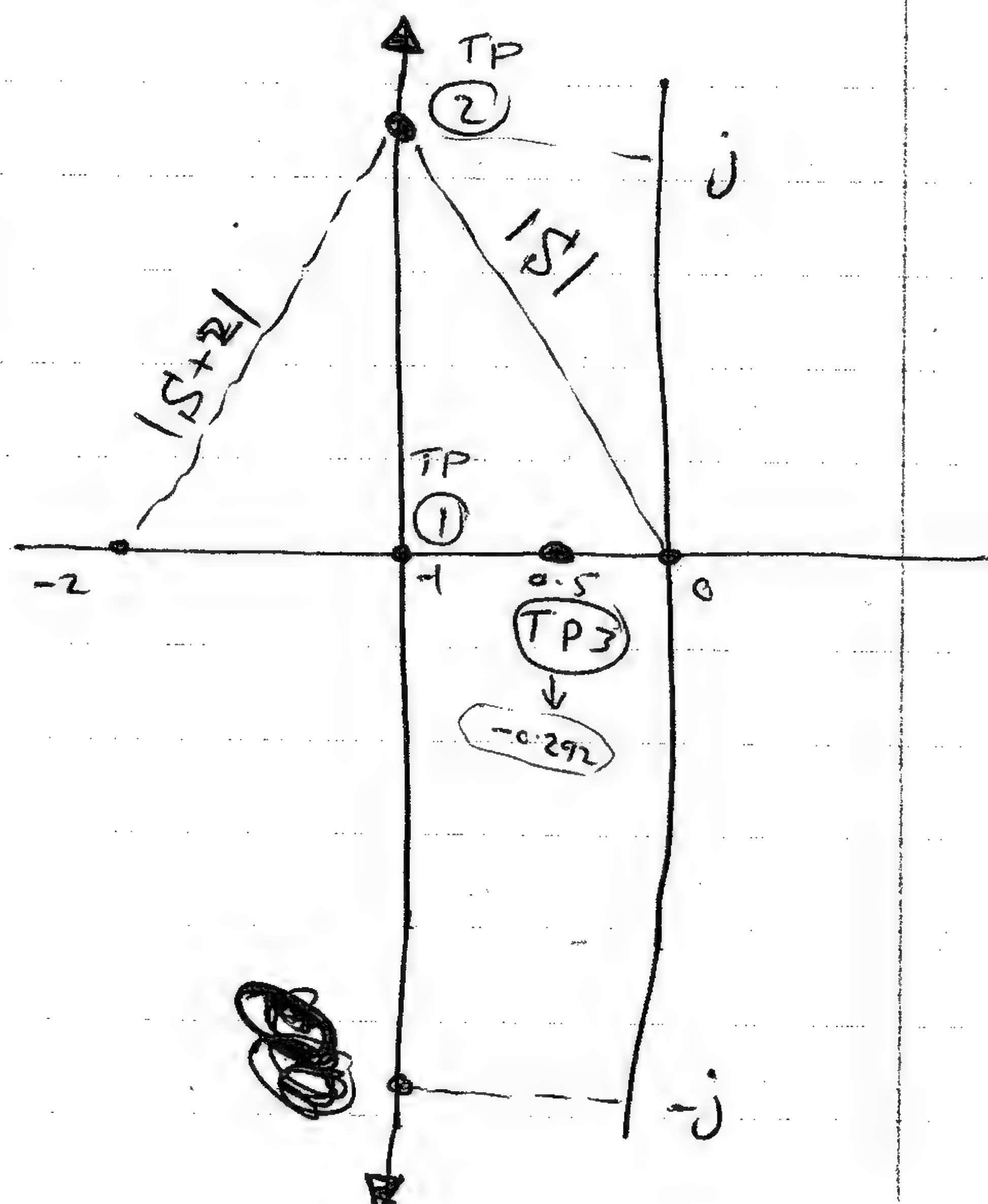
$$\Rightarrow \frac{k}{\sqrt{2} * \sqrt{2}} = \frac{2}{\sqrt{2} \sqrt{2}} = \frac{2}{2} = 1$$

③ at TP3 at $k=0.5$

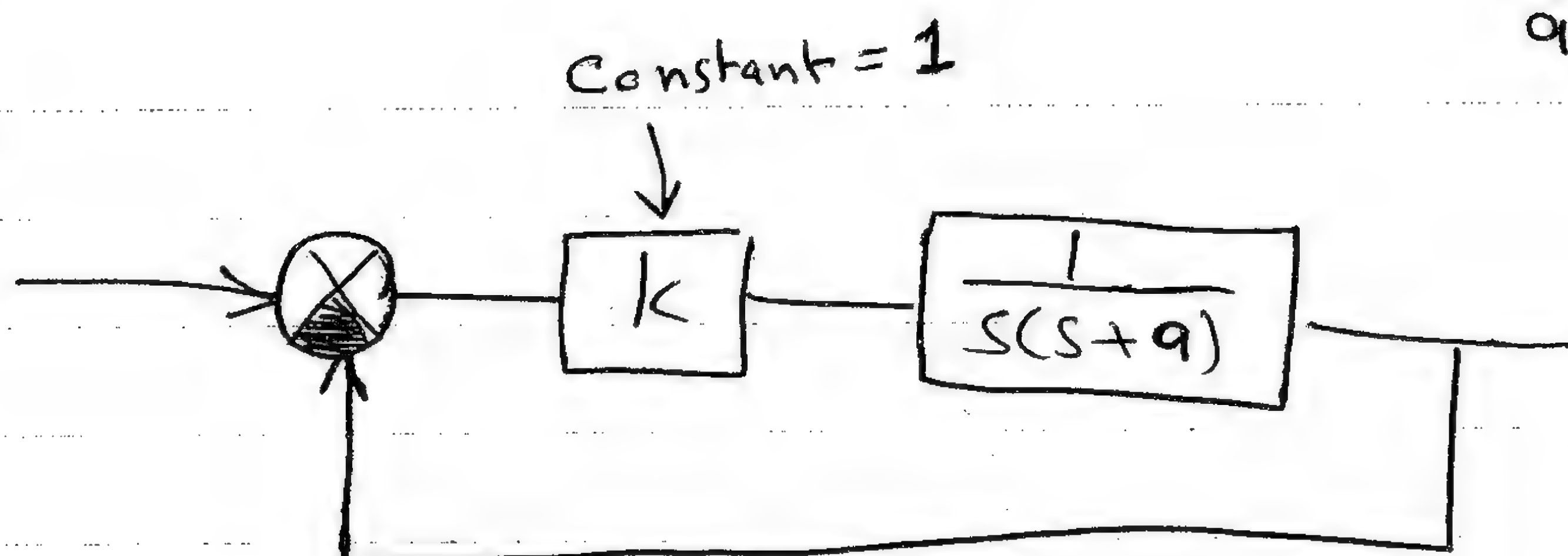
$$|s| = 0.292$$

$$|s+2| = 1.708$$

$$\Rightarrow \frac{k}{|s| |s+2|} = \frac{0.5}{|0.292| |1.708|} = 1.0025 \approx 1$$



Ex



k is constant
 a is Variable

$$KG(s) = -1$$

$$|KG(s)| = 1$$

$$\angle KG(s) = -180^\circ$$

but a is the Variable

$$aG(s) = -1$$

$$\angle aG(s) = -180^\circ$$

$$\Rightarrow \frac{-\frac{1}{s(s+a)}}{1 + \frac{1}{s(s+a)}}$$

$$\Rightarrow \frac{1}{s(s+a)} + 1 = 0$$

$$1 + s^2 + sa = 0$$

$$as + s^2 + 1 = 0 \quad \div s^2 + 1$$

$$a \frac{s}{s^2 + 1} + 1 = 0$$

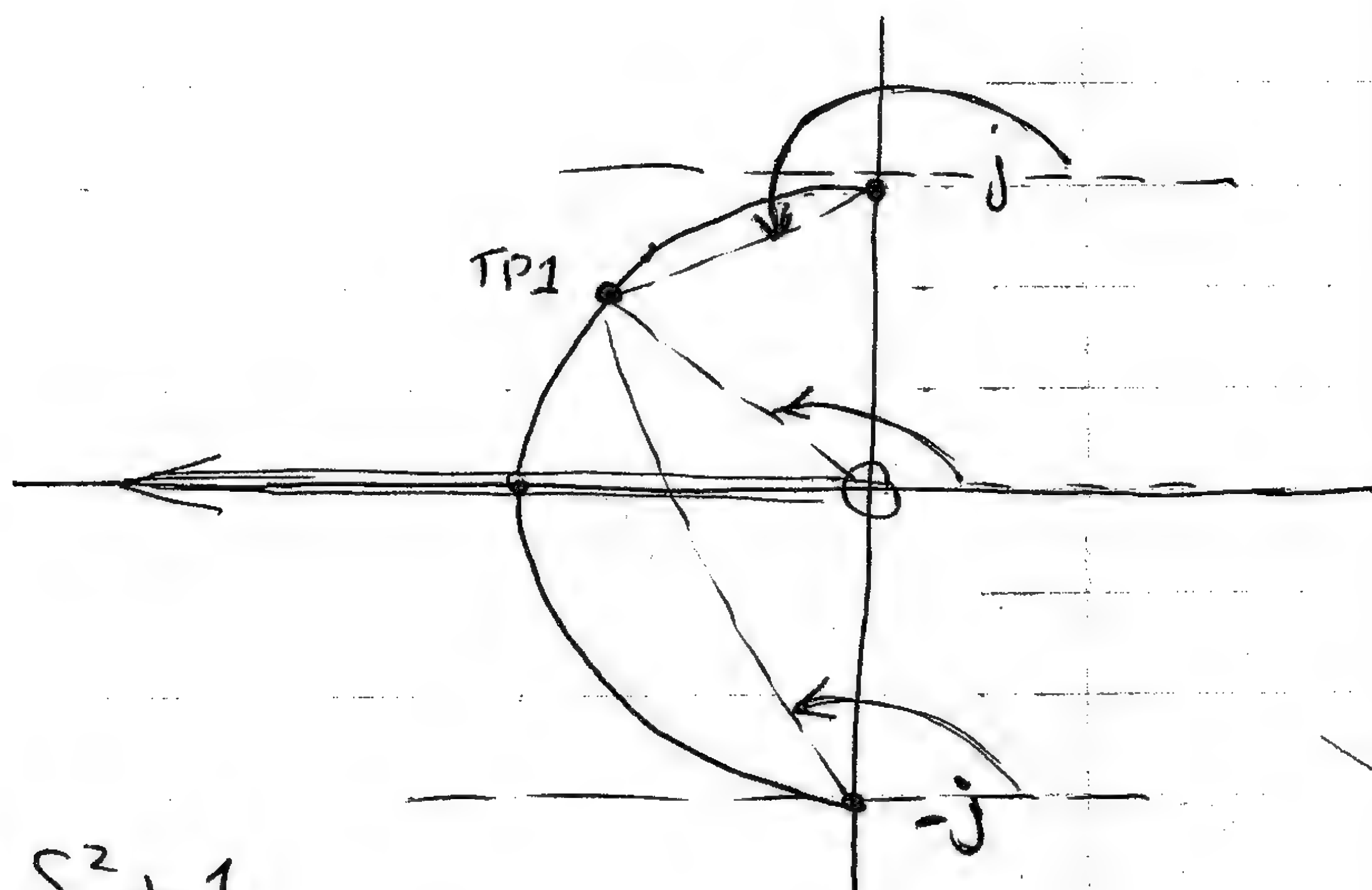
$$\Rightarrow a \frac{s}{s^2 + 1} + 1 = 0$$

$$\left| \frac{as}{s^2 + 1} \right| = 1 \Rightarrow$$

$$\frac{a |s|}{|s+j| |s-j|}$$

$$\angle \frac{as}{s^2 + 1} = -180^\circ \Rightarrow$$

$$-180^\circ = |s| - |s+j| - |s-j|$$



Root Locus Procedures

STEP 1 Write the characteristic equation as

$$1 + F(s) = 0$$

Then arrange the equation so that the parameter of interest appears as the multiplying factor $1 + Kp(s) = 0$

note : in most cases, $F(s) \neq Kp(s)$

$$1 + \frac{s}{s+a} = 0$$

$\rightarrow F(s)$

$$s + a + s = 0$$

$$2s + a = 0 \quad / 2s$$

$$1 + \frac{a}{2s} = 0$$

$$1 + a p(s)$$

STEP 2 Write the polynomial in the form of Poles & Zeros

$$1 + K \frac{\prod_{i=1}^m (s + z_i)}{\prod_{j=1}^n (s + p_j)}$$

STEP 3 Locate the poles & Zeros on the s-Plane with Selected Symbols as K Varies from $0 \rightarrow \infty$

pole	X
Zero	O

المعادلة = $\frac{1}{s}$

Ex Rewrite the equation in the following form :-

$$\prod_{i=1}^n (s + p_i) + K \prod_{i=1}^m (s + z_i)$$

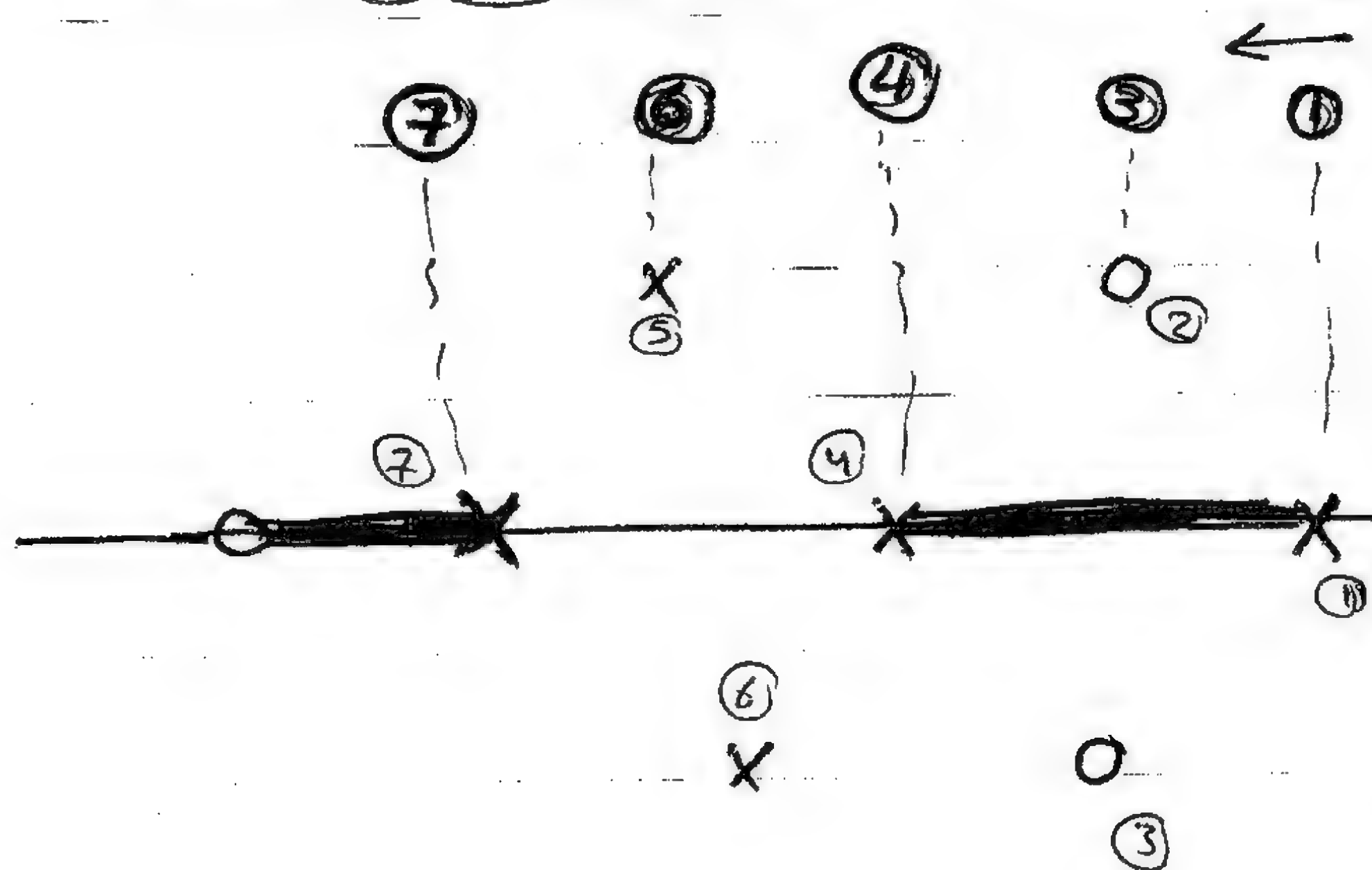
When $K=0 \Rightarrow$ The roots of ch. equ. are simply the poles of $P(s)$.

When $K=\infty \Rightarrow$ The roots of ch. equ. are simply the zeros of $P(s)$.

* There is $n-m$ branches of the root Locus approaches ∞

STEP 4 Locate the segment of the real-axis that are root Loci

"The root Locus on the real-axis always lies in a section of the real-axis to the left of an odd number of poles & zeros"



مبدأ اختيار المسار (يجب أن يكون مجموع الأقطاب

والمزادات (zeros) إذا وجدنا العدد فردياً ،

يكون هناك مسار Root locus عبه ،

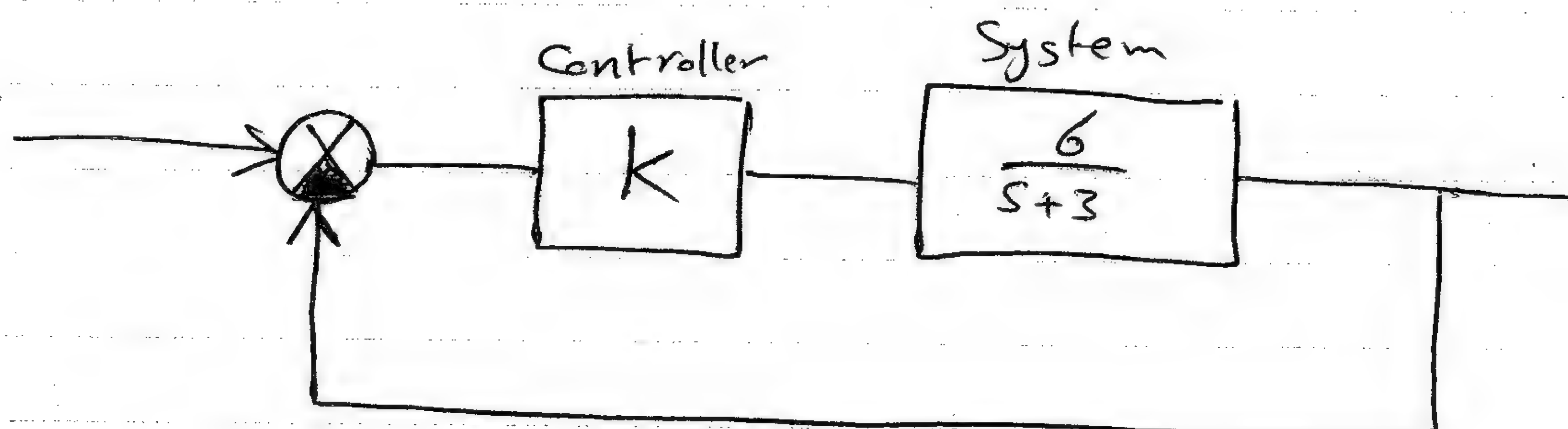
فضل ممرين في المسار

من الممرين إلى المسار ،

إذا أصبح مجموع الأقطاب والامتداد زوجي ،

لا يكون هناك مسار عبه ، وهكذا .

Example :- plot the root Locus of the following system as k varies from zero to ∞ .



$$T(s) = \frac{\frac{6k}{s+3}}{1 + \frac{6k}{s+3}}$$

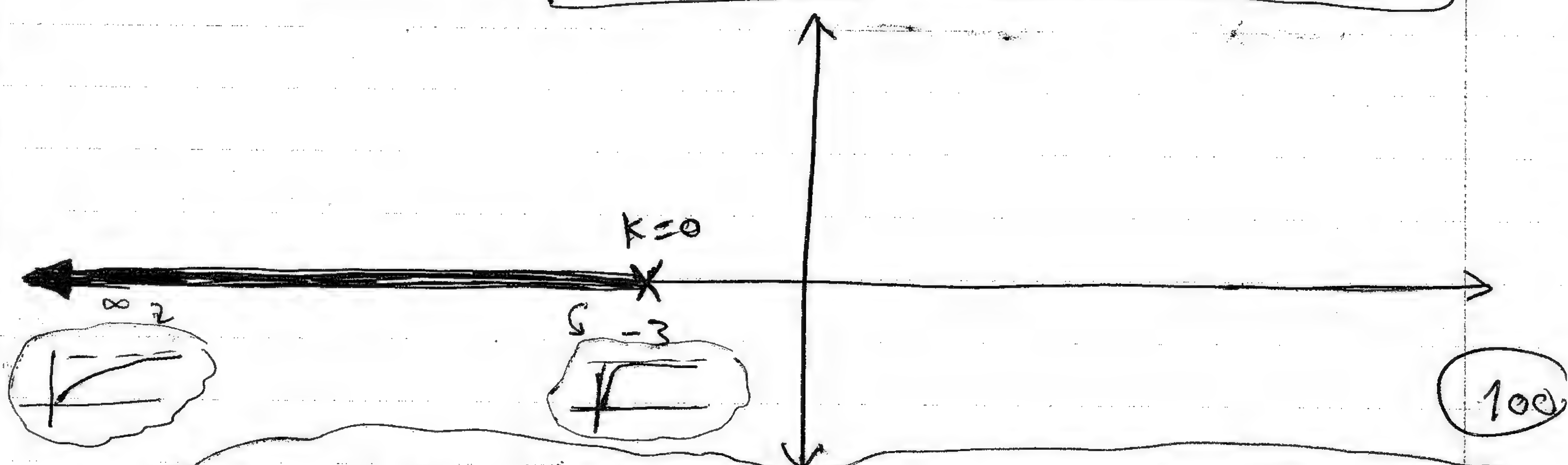
STEP 1 $1 + \frac{6k}{s+3} = 0 \equiv 1 + F(s) = 0$

STEP 2 $1 + K \frac{6}{s+3} = 0$ ← حاسة منا
مدقة زبط

STEP 3 $1 + K \frac{6}{(s+3)}$

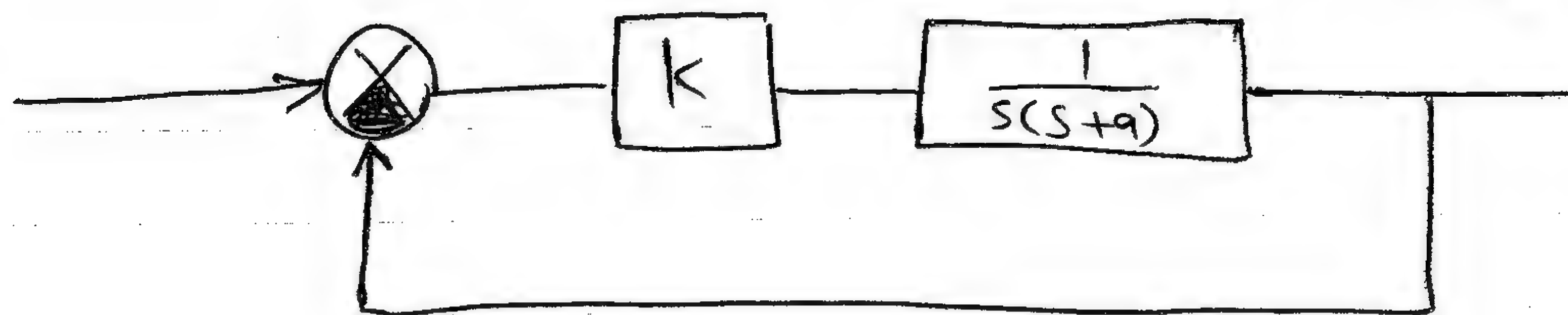
STEP 4 Poles $\Rightarrow S = -3$

Zeros \Rightarrow Not available, but there is one goes to ∞



ملاحظة :- اذا كان نظام من الدرجة الاولى ، فخطوات الأربعة الأولى كافية لرسم Root Locus.

Ex :-



$$T(s) = \frac{\frac{k}{s(s+a)}}{1 + \frac{k}{s(s+a)}}$$

STEP 1 : $1 + F(s) = 0$

$$1 + \frac{k}{s(s+a)} = 0$$

STEP 2 : $1 + \frac{k}{s(s+a)} = 0$

$$1 + a p(s) = 0$$

$$s(s+a) + k = 0$$

$$s^2 + as + k = 0$$

$$s^2 + k + as = 0 \quad \div (s^2 + k)$$

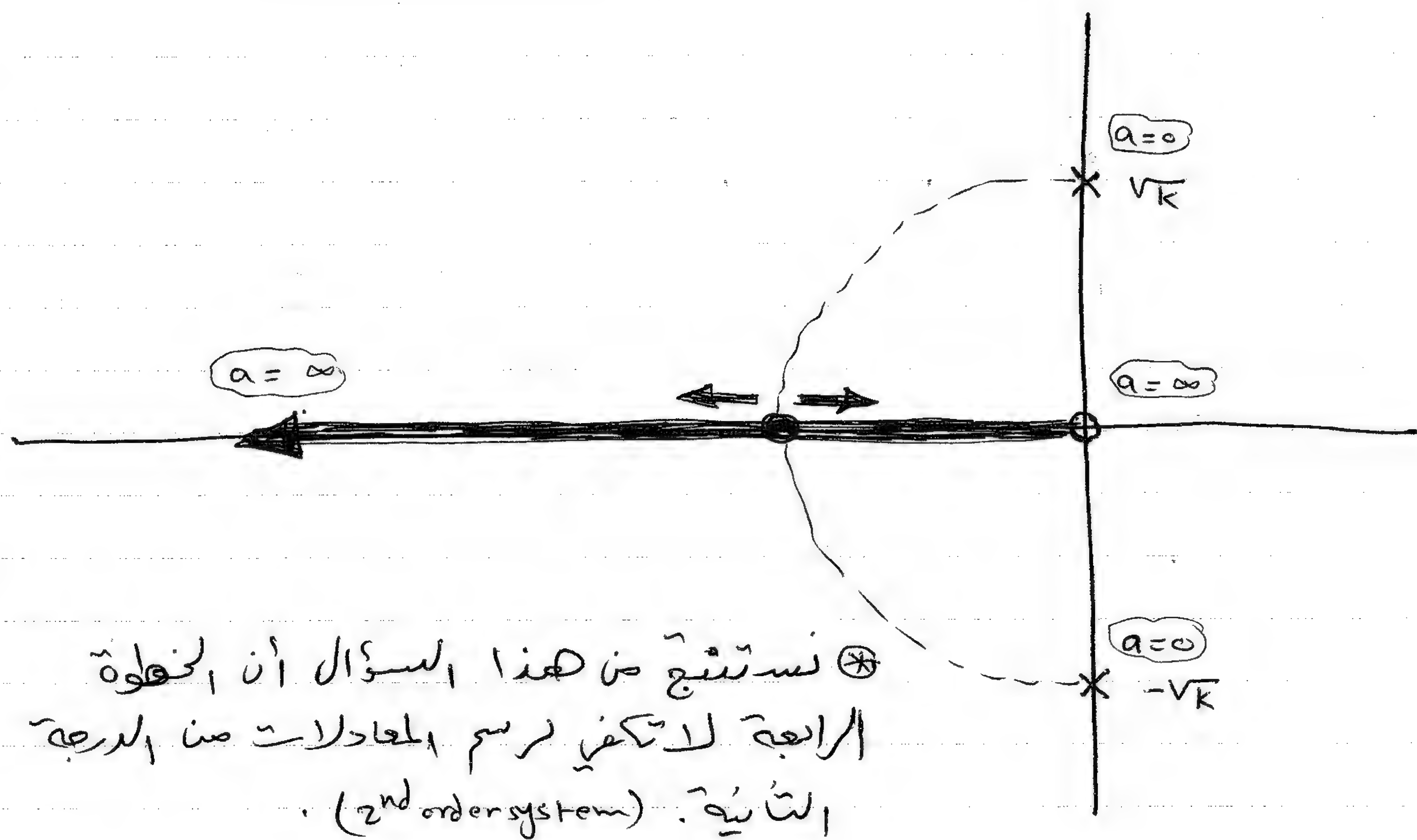
$$\Rightarrow \left[1 + \frac{as}{s^2 + k} \right] \rightarrow 1 + a p(s) = 0$$

أصبحت على صورة القياسية

STEP 3 : $1 + a \frac{s}{s^2 + k} = 0 \Rightarrow 1 + a \frac{s}{(s+j\sqrt{k})(s-j\sqrt{k})} = 0$

STEP 4 :- Poles : $s = \pm j\sqrt{k}$
Zeros : $s = 0$

Pole conjugate always symmetrical



Back To General STEPS - [عودة الخطوات الرئيسية]

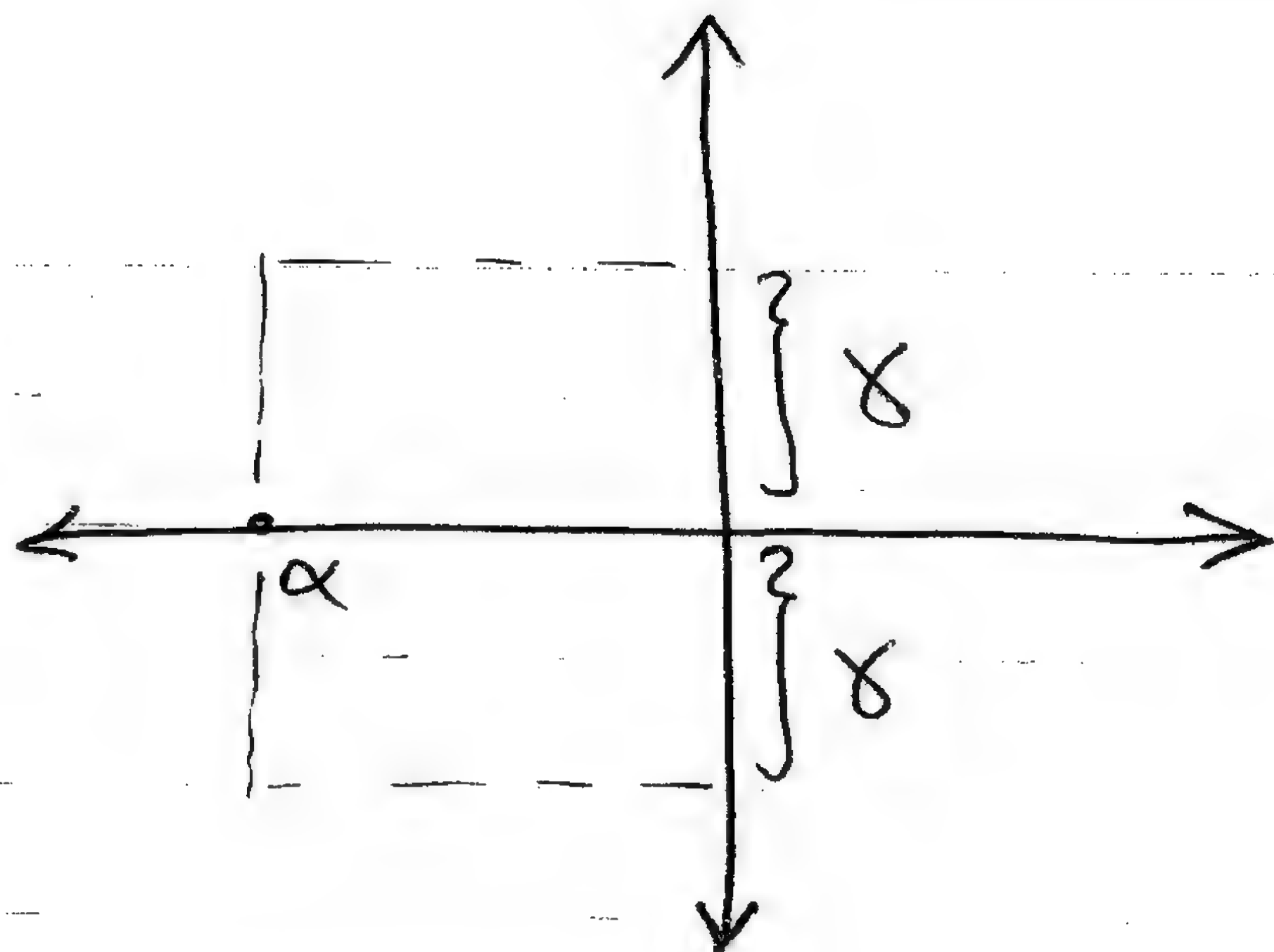
STEP 5 Determine the number of separate loci

$$\text{No of Separate Loci} = \text{No of Poles}$$

STEP 6 The root Loci must be symmetrical with respect to the horizontal real-axis, because the complex roots must appear as pole conjugate.

$$S_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} = \frac{-b}{2a} \pm \frac{j9}{2a} = \alpha \pm j\gamma$$

$$\alpha + j\gamma \rightarrow$$



STEP 7 The Loci proceeds to the zero at ∞ along asymptote centered at σ_A , and with angle ϕ_A , when the N_0 of ~~poles of $P(s)$~~ finite zeros of $P(s)$ is less than the N_0 of poles of $P(s)$

$N_z < N_p$ Then we have N_0 of zeros at ∞

$$N = N_p - N_z$$

These Linear asymptotes are centered at a point on the real axis & given by :-

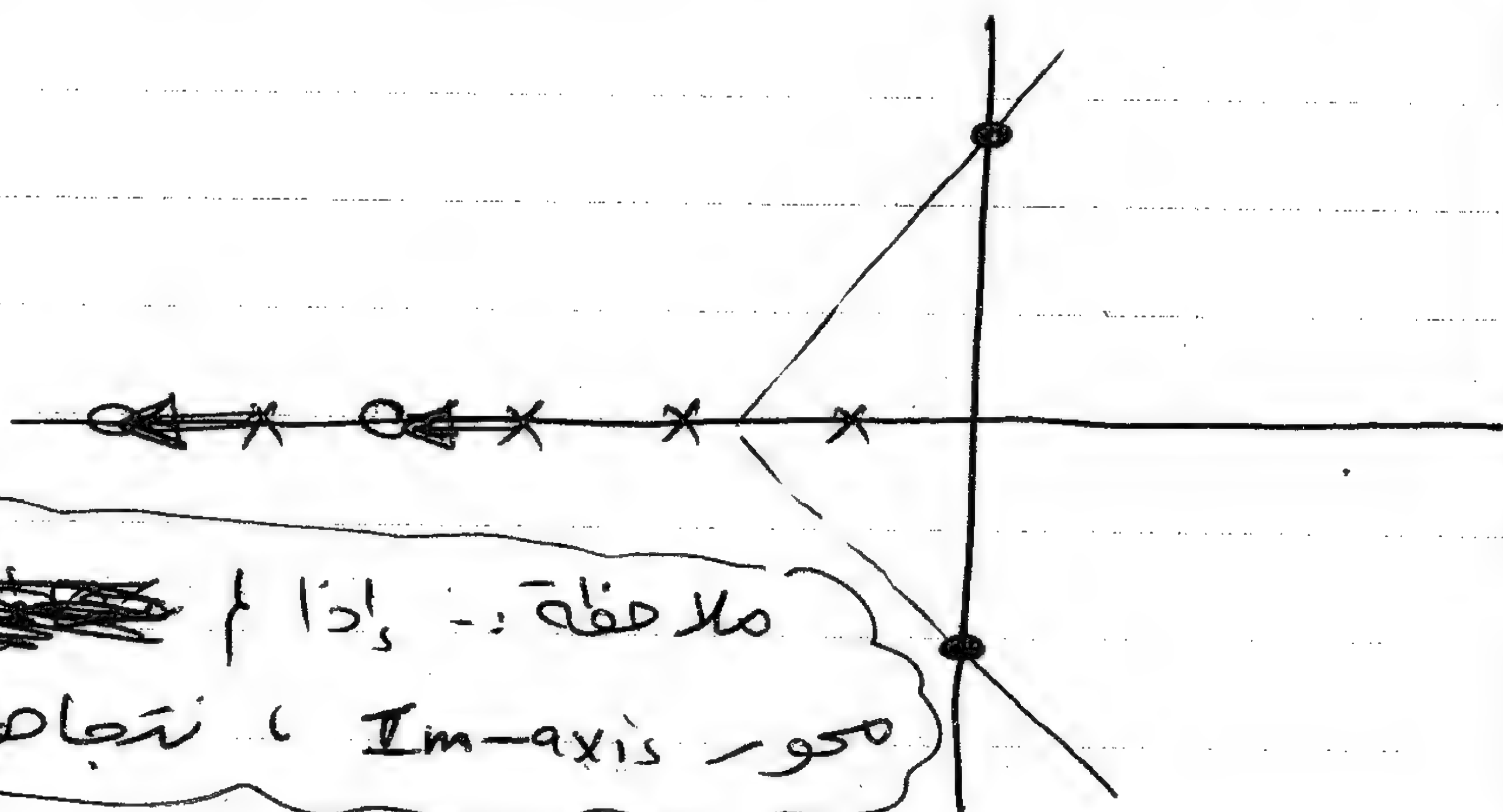
$$\sigma_A = \frac{\sum \text{Poles of } P(s) - \sum \text{Zeros of } P(s)}{N_p - N_z}$$

* The angle of asymptotes with respect to real axis is given by :-

$$\phi_A = \frac{2q + 1}{N_p - N_z} * 180 \quad q = (0, 1, 2, 3 \dots N_p - N_z - 1)$$

STEP 8

Determine the point of which the root Locus Crosses the Imaginary-axis (Use Routh Hurwitz Criteria)

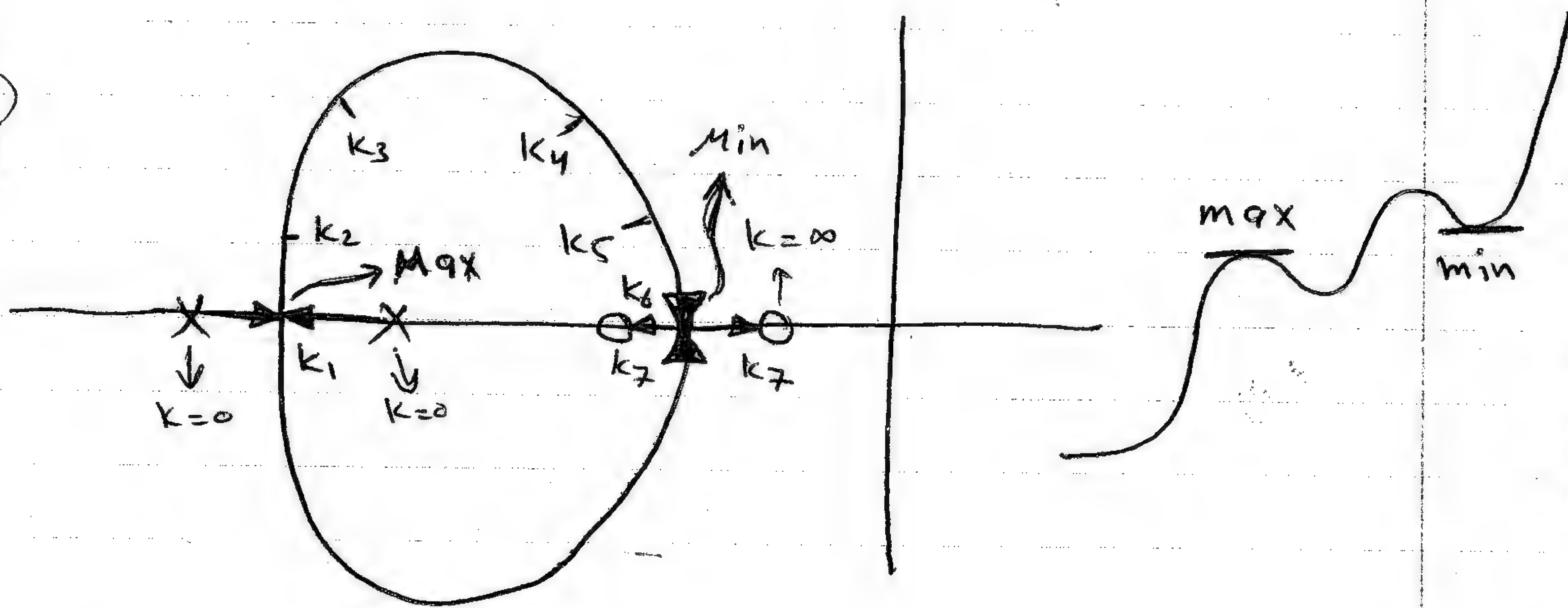


ملاحظة: إذا لم يكن هناك تقاطع مع Im-axis، نتجاهل النقطة ω_c .

STEP 9

Determine the Break-away & Break-in points.

X : Pole
O : Zero



① Put or Find the equation of k

$$1 + kP(s) = 0 \Rightarrow k = \frac{-1}{P(s)}$$

② Find $\frac{dk}{ds} = 0$

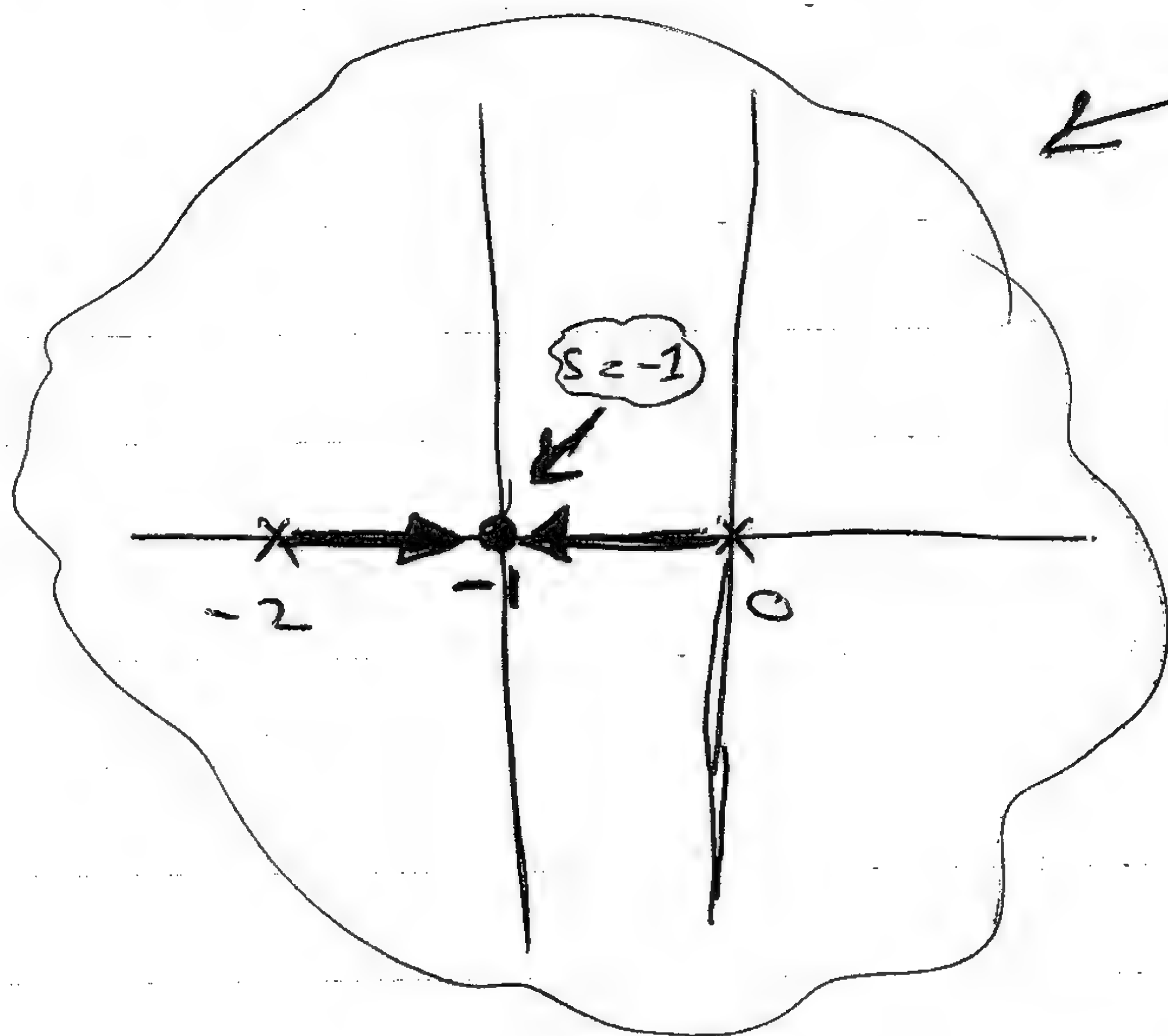
Ex

$$1 + \frac{k}{s(s+2)} = 0$$

$$k = -s(s+2)$$

$$k = -s^2 - 2s$$

$$\frac{dk}{ds} = -2s - 2 = 0 \Rightarrow -2s = 2 \Rightarrow \boxed{s = -1}$$

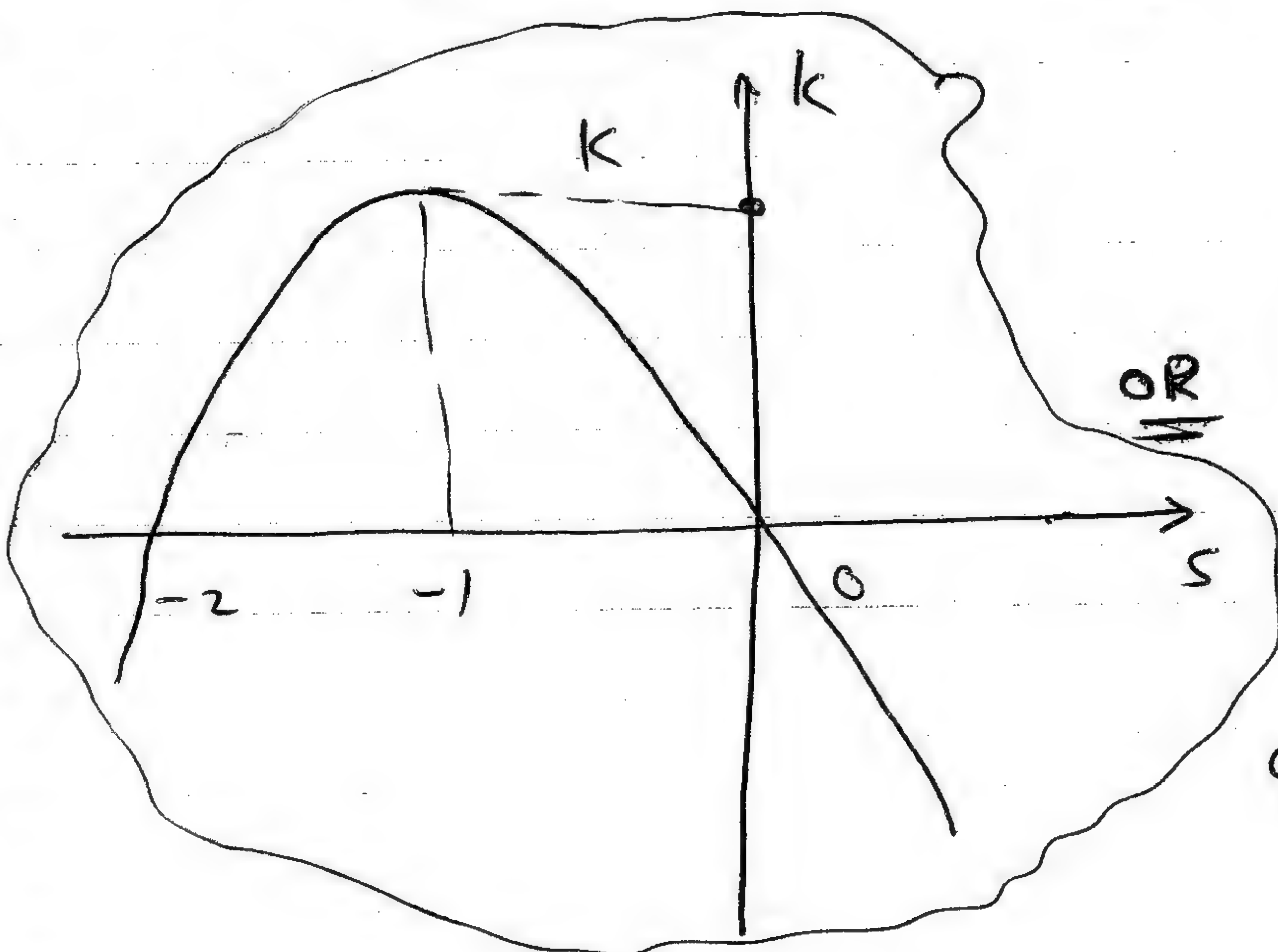


طرق حل الخطوة التاسعة

① ايجاد المشتقة $\frac{dk}{ds} = 0$

② ايجاد Table لليجاد قيم min و max الخاصة بـ k

③ ايجاد صغرى لليجاد قيم min و max الخاصة بـ k



OR

s	0	-1	-2	-3
k	0	1	0.2	0.1

OR

$$\frac{dk}{ds} = 0$$

Ex Find the root Locus of the following system

$$1 + \frac{K}{(s+2)(s+4)} = 0$$

- **STEP 1** already done.

- **STEP 2** already done.

STEP 3 Poles : $s = -2$ $s = -4$

STEP 4 determine the Loci Segment.

STEP 5 No of Loci = 2.

STEP 6 will be taken in consideration.

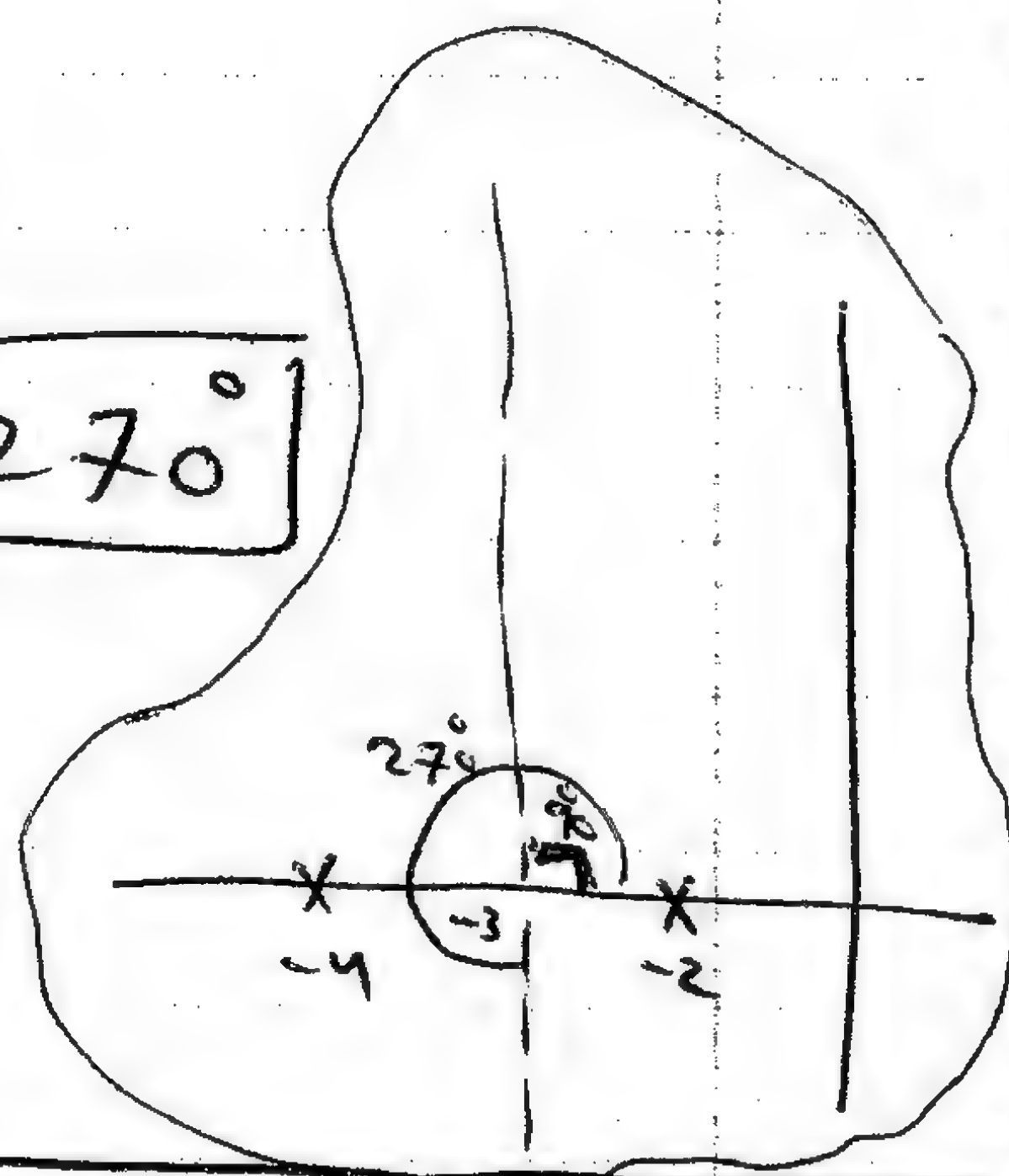
$$\begin{aligned} \text{STEP 7 } \phi_A &= \frac{\sum \text{Poles} - \sum \text{Zeros}}{N_P - N_Z} = \frac{-2 - 4 - (0)}{2 - 0} \\ &= \frac{-6}{2} = \boxed{-3} \end{aligned}$$

$$\phi_A = \frac{2q+1}{2} * 180 \quad ; \quad q = 0, 1$$

$$\phi_A = \frac{2(0)+1}{2} * 180 = \frac{1}{2} * 180 = \boxed{90^\circ}$$

$$\phi_A = \frac{2(1)+1}{2} * 180 = \frac{3}{2} * 180 = \boxed{270^\circ}$$

$$\therefore \phi_A = 90^\circ, 270^\circ$$



STEP 8 No intersect with Imaginary axis

STEP 9 $k = -(s+2)(s+4)$

$$K = -s^2 - 6s - 8$$

$$\frac{dL}{ds} = -2s - 6 = 0 \Rightarrow -2s = 6 \Rightarrow \boxed{s = -3}$$

Sentraid أنت أنت أنت Breakway ~~Breakway~~ أنت أنت أنت

إذا \hat{u} line تقعين \hat{u}
 $S = -3$
 $S = -5$

(Breakaway واحد من كتل

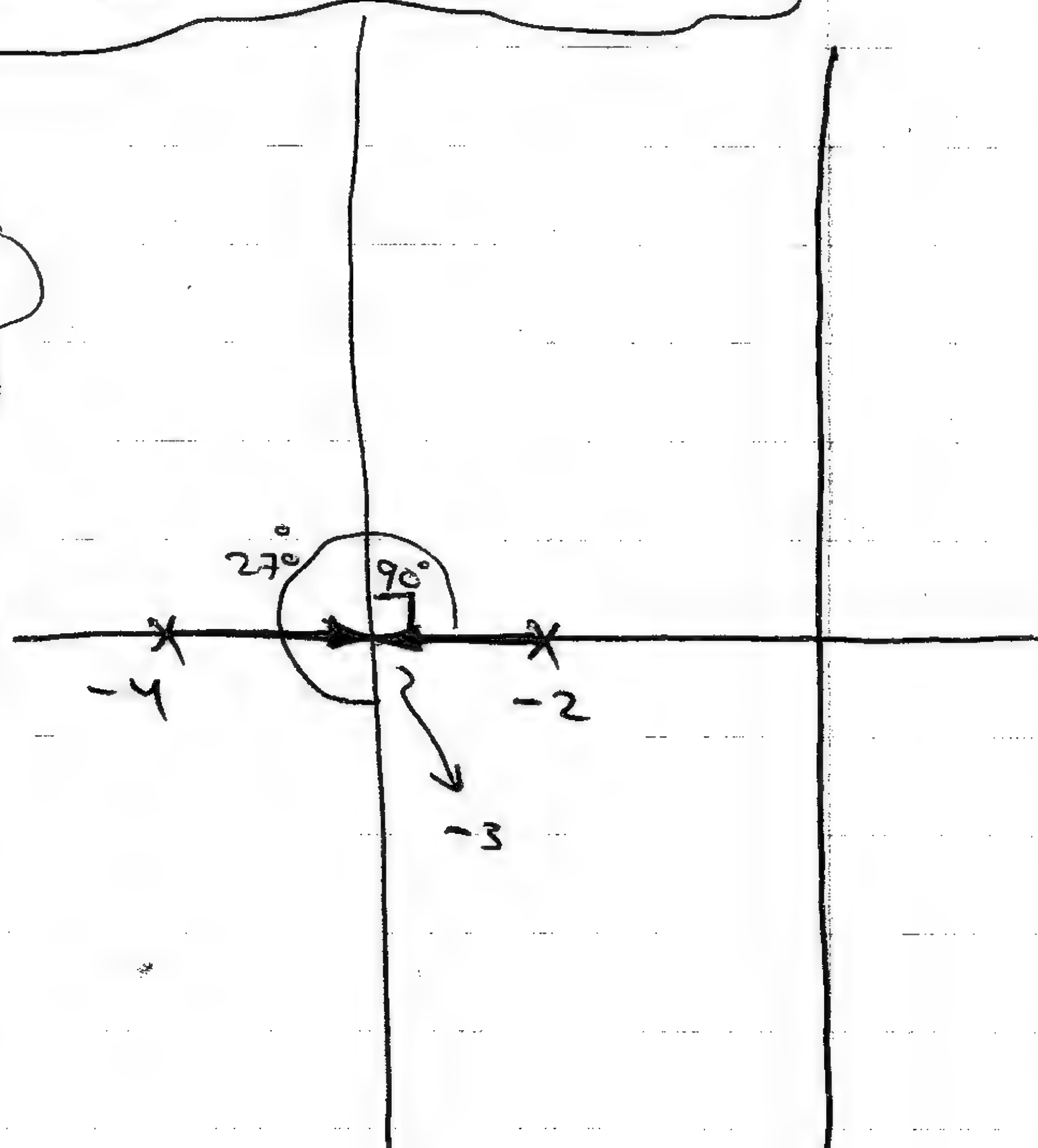
Break in والاخرى سكون

کیف حرف ذلہ ؟

نحوه ۵ و ۶ الی

فتیہ کا مراتب سے Breakaway

Break in قِصَّة | الاصغر



Ex Find the root Locus of the following systems

$$1 + k \frac{(S+1)}{S(S+2)(S+4)^2} = 0$$

R	0	0.412	0.42	0.417	0.39
S	-2	-2.4	-2.45	-2.5	-2.1

STEP 1) already done

STEP 2 already done

STEP 3 Poles: $S=0, -2, -4, -4$

Zeros: $S = -1$

STEP 4 Locating segments on real-axis

STEP 5 :- No of Separate Loci = No of poles = 4

STEP 6 To be Taken in Consideration

STEP 7 $\phi_A = \frac{\sum \text{Poles} - \sum \text{Zeros}}{N_P - N_Z} = \frac{0 - 2 - 4 - 4 - (-1)}{3} = \boxed{-3}$

$\phi_A = \frac{2q+1}{N_P - N_Z} * 180$, $q = 0, 1, 2$

$\phi_A = \frac{2q+1}{3} * 180 \Rightarrow \phi_A = \underline{60}, \underline{180}, \underline{300}$

STEP 8 $1 + \frac{k(s+1)}{s(s+2)(s+4)^2} = 0 \Rightarrow s(s+2)(s+4)^2 + k(s+1) = 0$

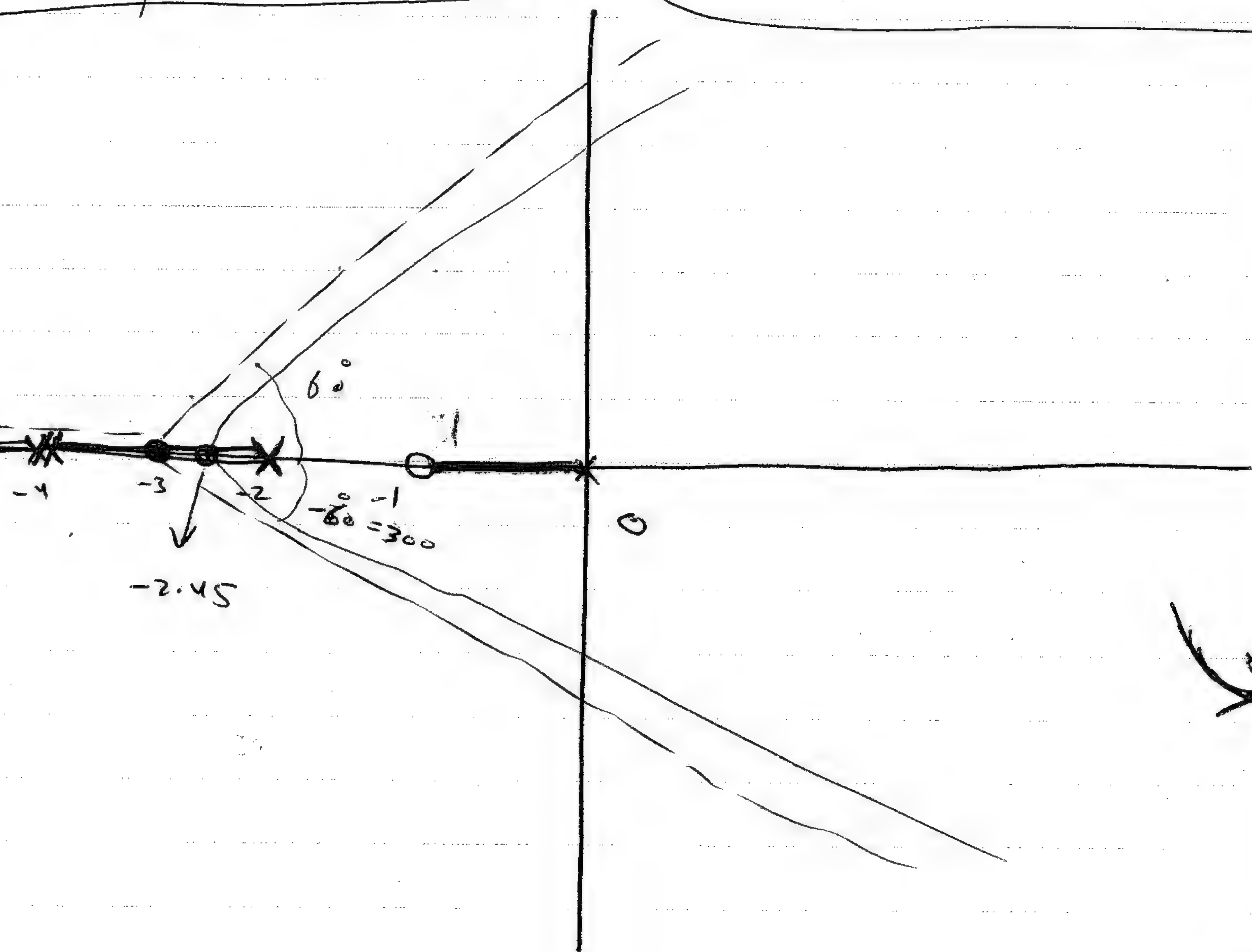
at Home

Im لايجاد متقاطع مع محور

s^4
 s^3
 s^2
 s^1
 1

$\frac{1-k}{0}$

Take this equation and find the intersection points with Imaginary-axis



Breakaway point is

STEP 9 $S = -2.45$

Back To General STEPS

STEP 10

Determine the angle of departure ^{بالفأرة} φ and the angle of arrival ^{الوصول} using the phase angle criteria.


$$\phi = \pm 180 (2\varphi + 1)$$

Take $\phi = \pm 180$ at $\varphi = 0$

180

Example $G.H(s) = \frac{k}{(s+p_3)(s^2 + 2\zeta\omega_n s + \omega_n^2)}$

$= \frac{k}{(s+p_3) \underbrace{(s+p_1)(s+p_2)}_{\text{Pole conjugate}}}$

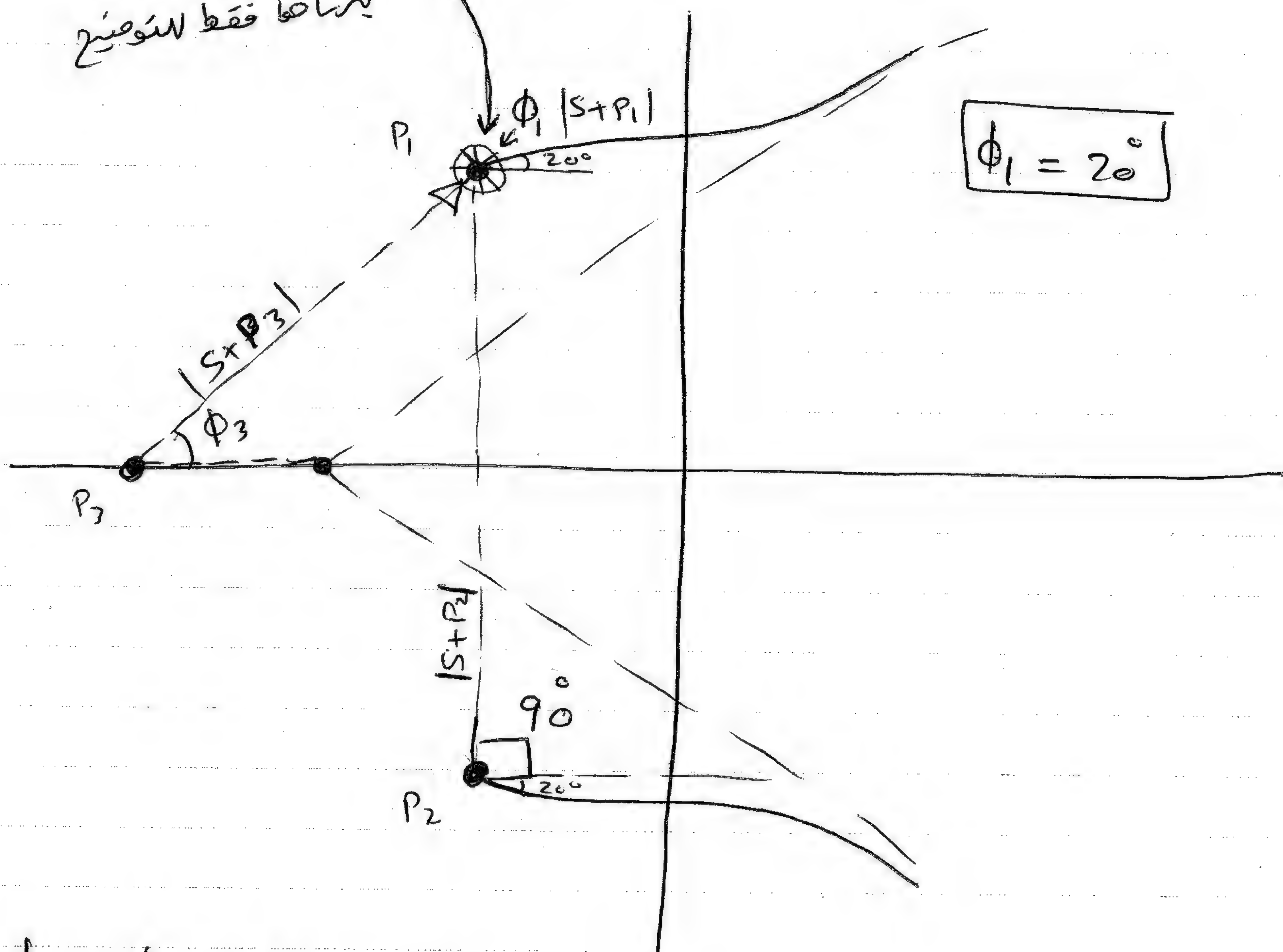


$$\phi_A = \frac{p_1 + p_2 + p_3}{3 - 0}$$

$$\phi_A = \frac{(2\varphi + 1)}{3} * 180 \quad (\varphi = 0, 1, 2)$$

$\phi = 60, 180, 300$

من عبارة عند دائرة نصف قطرها صفر
ليتنا فقط للتوضيح



$$\phi_1 + \phi_2 + \phi_3 = 180$$

$$\phi_1 + 90 + \phi_3 = 180$$

$$\phi_1 = 90 - \phi_3$$

Suppose that $\phi_3 = 70^\circ$ مجرد افتراض

$$\therefore \phi_1 = 90 - 70 = 20^\circ$$

angle of departure :



زاوية الانحدار
for poles

angle of arrival :



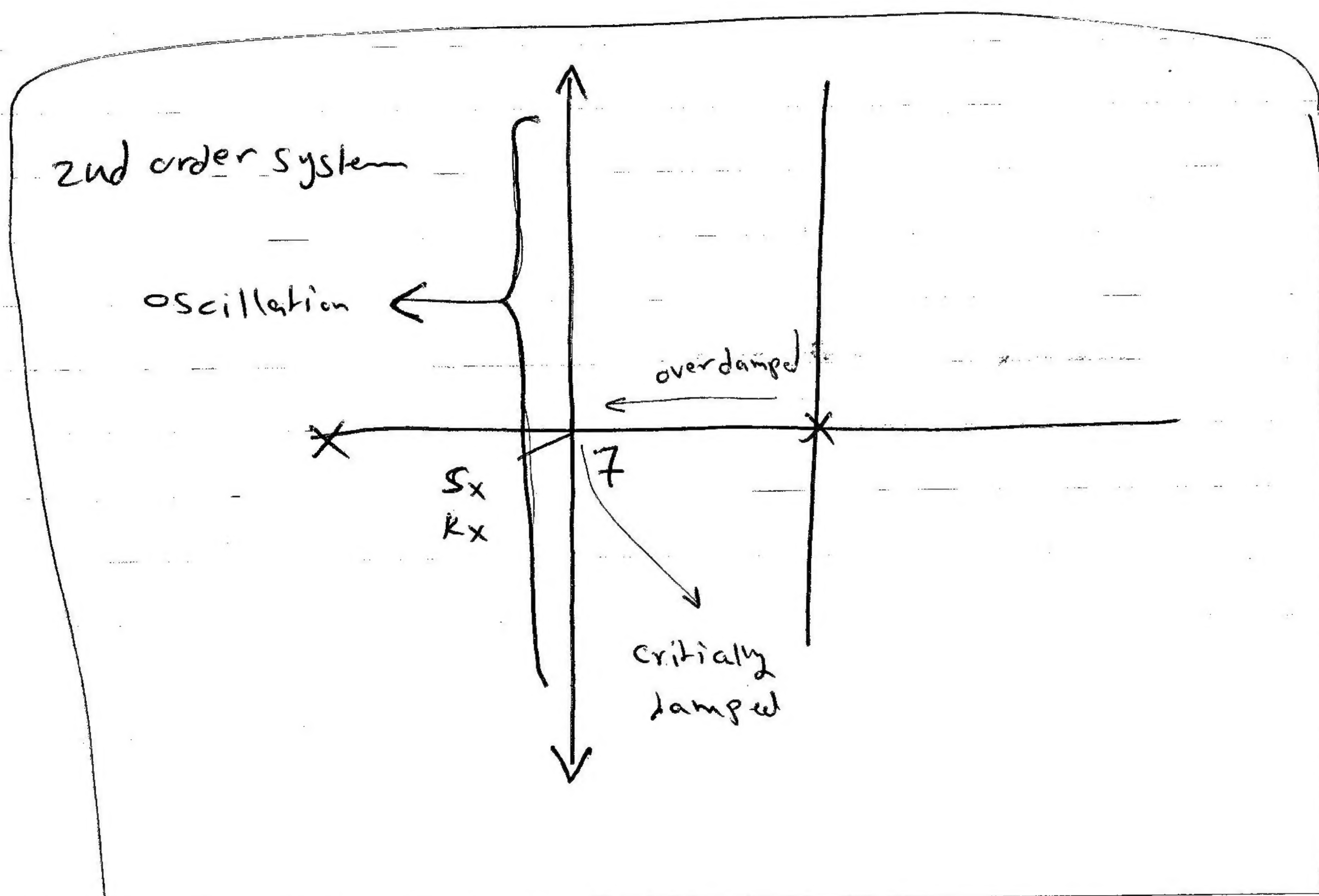
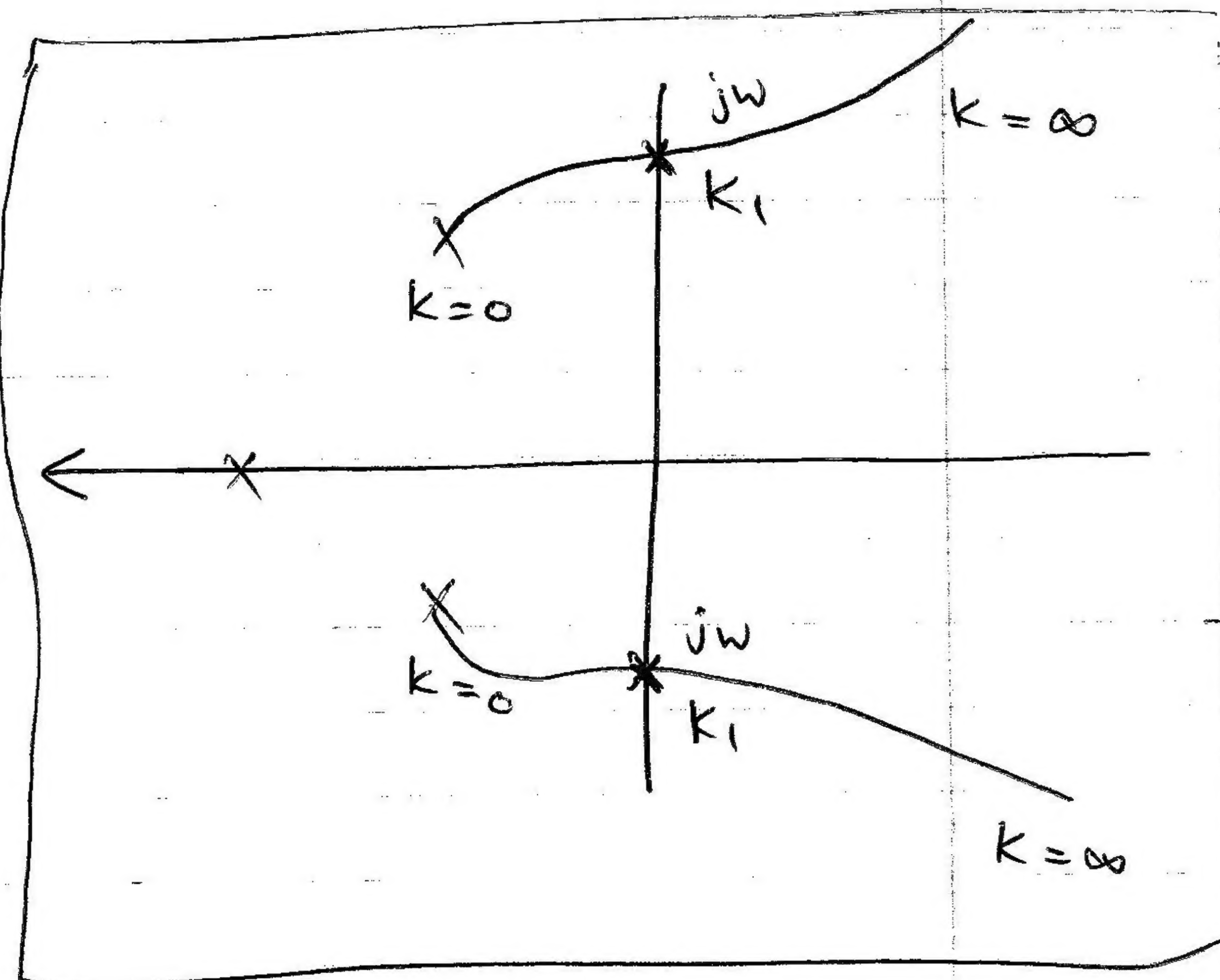
زاوية الوصول
for zeros

STEP 11 PLOT (take in consideration all the previous steps and plot the system).

STEP 12

Determine the parameter value k_x & specific root s_x

$$k = \frac{\prod_{j=1}^n (s + p_j)}{\prod_{i=1}^m (s + z_i)}$$



Example | plot the root locus for the ch. equ. as K varies from zero to infinity

$$G(s) = 1 + \frac{K}{s^4 + 12s^3 + 64s^2 + 128s}$$

STEP 1 DONE

STEP 2 DONE

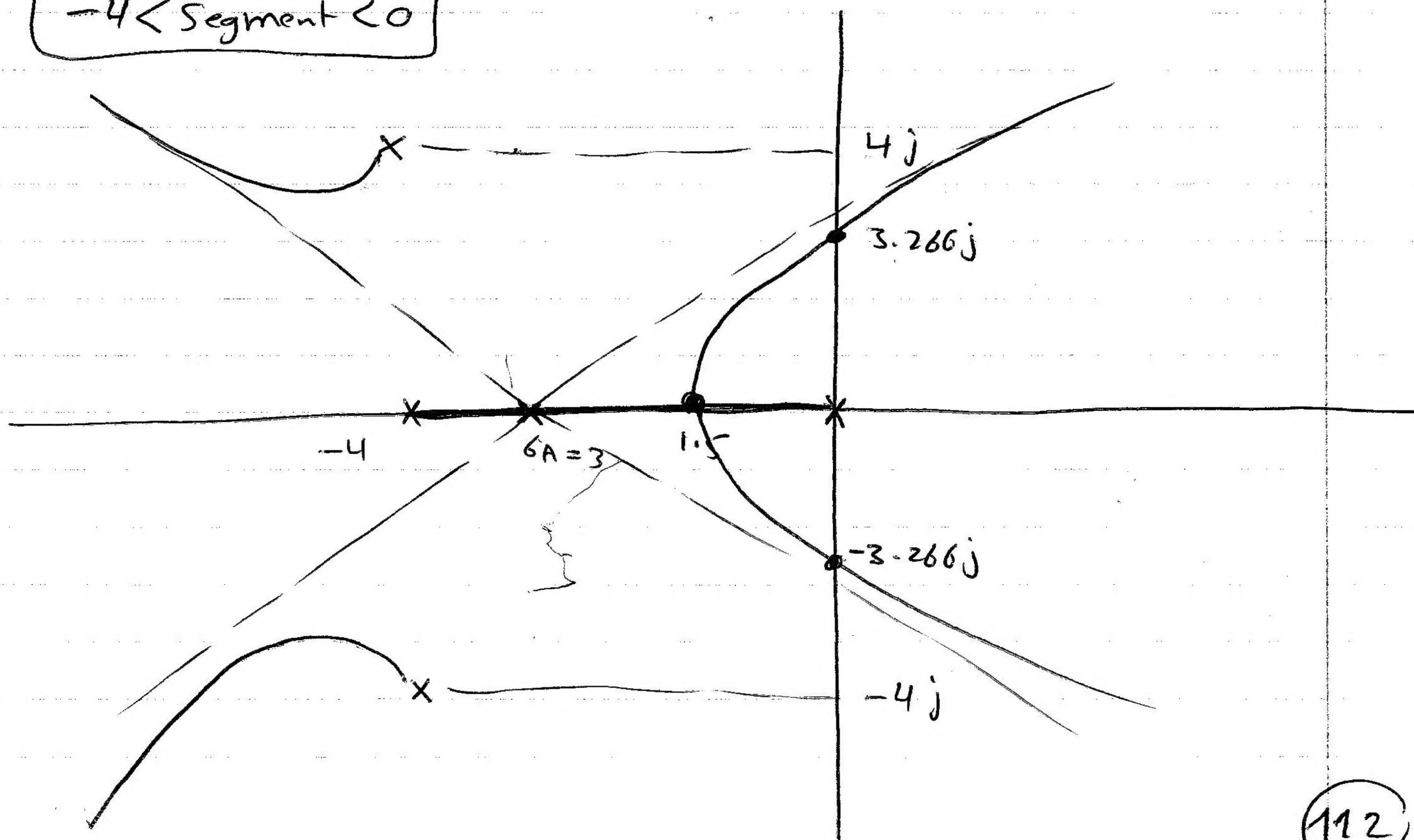
STEP 3 ~~NO ZEROS~~

~~Poles:~~ $1 + \frac{K}{s(s+4)(s+4+4j)(s+4-4j)}$

STEP 4 Zeros : No Zeros

Poles : $s = \underline{0}, \underline{-4}, \underline{-4-4j}, \underline{-4+4j}$

$-4 < \text{Segment} < 0$



STEP 5 Number of separate Loci = $N_p = 4$

STEP 6 σ To be taken in consideration.

STEP 7 $\phi_A = \frac{\sum \text{poles} - \sum \text{zeros}}{N_p - N_z} = \frac{-4 + -4 + -4 + 0}{4} = -3$
 $(q = 0, 1, 2, 3)$

$\phi_A = \frac{2q+1}{4-0}$

$\phi = 45^\circ, 135^\circ, 225^\circ, 315^\circ$

$q = 0 \quad 1 \quad 2 \quad 3$

STEP 8 ch. equ. $q(s) = s^4 + 12s^3 + 64s^2 + 128s + k = 0$

s^4	1	64	k
s^3	12	128	0
$\rightarrow s^2$	53.33	k	0
s^1	C_1	0	
1	k		

Auxiliary equation

C_1 must be zero $\Rightarrow k = 568.89$

\therefore Auxiliary Equation :-

$53.33 s^2 + 568.89 = 0 \Rightarrow s_{1,2} = \pm j 3.266$

STEP 9

k	0	75	85	80	68	51	0
s	0	-1	-1.5	-2	-2.5	-3	-4

STEP 10 Angle of Departure $\Phi = 225^\circ$

STEP 11 Plot (go back to the plot page 112)

STEP 12



Stable for $0 < K < 568.89$

اے کی دنیا امتحان ہو سکتی

بالوفیق للجميع



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